

BAB V

KESIMPULAN DAN SARAN

5.1. Kesimpulan

Dari hasil analisis struktur bangunan Gedung Bank NTB Syariah dengan menambahkan dinding geser terhadap penempatannya dapat disimpulkan beberapa hal, yaitu :

1. Berdasarkan hasil analisis ketiga pemodelan yang ada, dapat disimpulkan bahwa penempatan posisi dinding geser (*Shear Wall*) lebih efektif jika diletakan pada bagian sudut siku gedung, apabila jika ditinjau dari hasil nilai simpangan pada arah x dan y.
2. Dari masing-masing alternatif 1, 2, dan 3 simpangan arah x sebesar 0,00022 dan arah y sebesar 0,000412 untuk alternatif 1, simpangan arah x sebesar 12,3833 arah y 1,8678 untuk alternatif 2, dan simpangan arah x 1,557 arah y 6,9811 untuk alternatif 3 pada lantai 1. sedangkan gaya geser maksimum terkecil pada kolom lantai 2 terjadi pada dinding geser alternatif 1 dimana gaya geser maksimumnya sebesar 119,073 kN.m dan momen maksimum terkecil terjadi pada dinding geser alternatif 1 dimana momen maksimumnya sebesar 9,517kN.m. Dari ketiga model diatas didapatkan yang paling efektif adalah alternatif 1 dengan penempatan posisi pada bagian sudut siku gedung.

5.2. Saran

Berdasarkan kesimpulan diatas, ada beberapa saran yang dapat disarankan yaitu :

1. Dalam analisis ini banyak faktor yang tidak diikut sertakan seperti, perencanaan pondasi, pengaruh dinding terhadap kekakuan dan lain-lain, sehingga diperlukan penelitian lebih lanjut dengan mengikutsertakan faktor-faktor lainnya.
2. Dalam analisis ini yang digunakan hanya metode Analisa dinamik respon spektrum, untuk penelitian lebih lanjut dapat mempertimbangkan metode analisis dinamik riwayat waktu (*time history*) sebagai perbandingan dari analisis ini.

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JUDUL TUGAS AKHIR

Pengaruh Penempatan Dinding Geser Terhadap
 Perilaku Struktur Gedung Bank NTB Syariah
 Mataram

DOSEN PEMBIMBING

Pembimbing I

Dr.Eng. Hariyadi,ST., M.Sc (Eng)
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Pembimbing II

Ahmad Zarkasi, ST., MT.
 NIDN.0819068903

NAMA MAHASISWA

Ranni Sahlinda
 NIM.2019D1B161

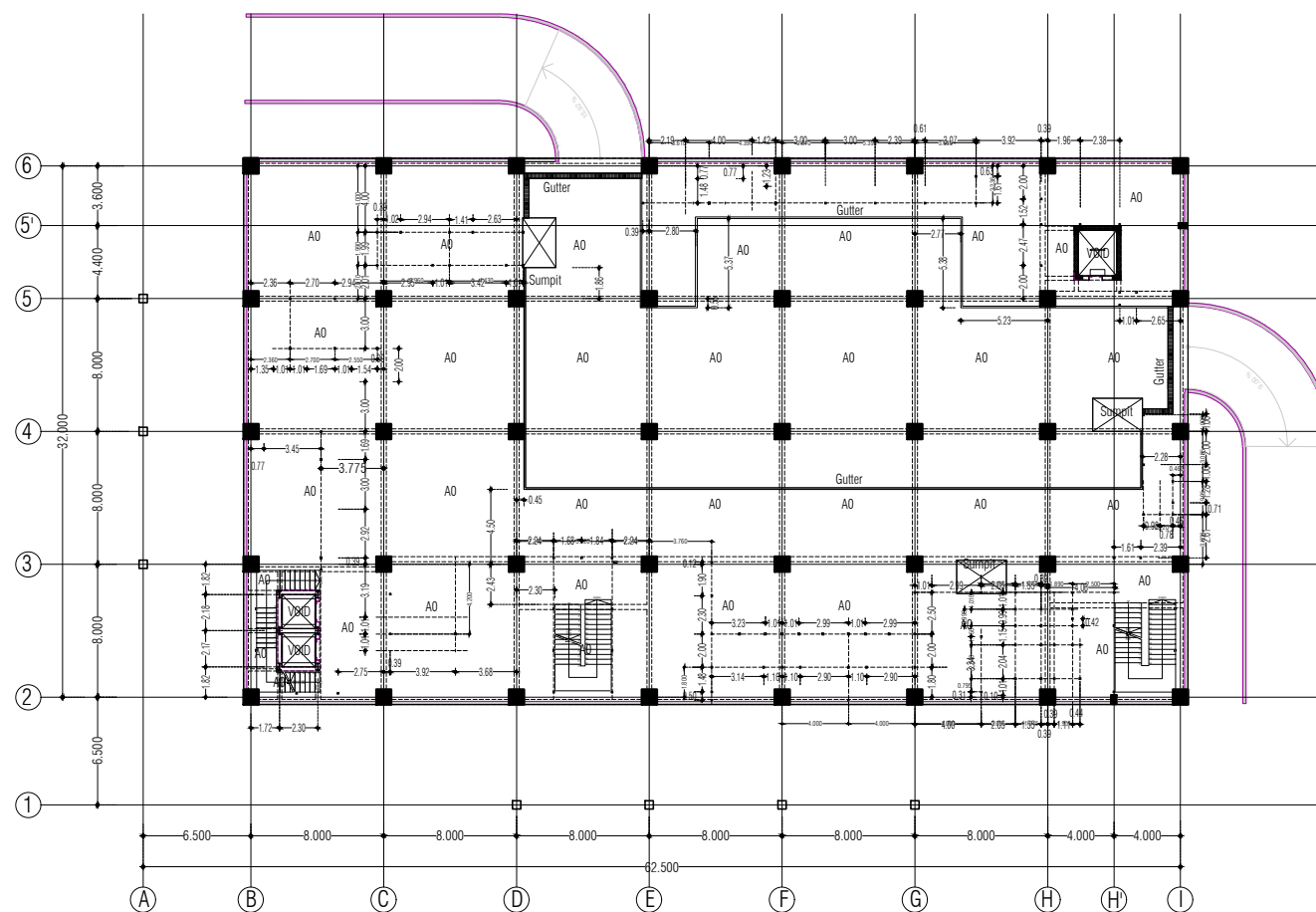
KETERANGAN

DENAH PLAT LANTAI BASEMENT
 (SFL - 3.900)

JUDUL GAMBAR

SKALA NO. GAMBAR JML. GAMBAR

1 : 250



DENAH PLAT LANTAI BASEMENT (SFL -3.900)

SKALA 1 : 250

LEGENDA GAMBAR

| NOTASI | TEBAL PLAT | TULANGAN | NOTASI | TEBAL PLAT | TULANGAN |
|--------|------------|---|--------|------------|---|
| A0 | 120 | Tul. Wiremesh # # M8 -150 (2 lapis) | A2 | 120 | Tul. Memendek # # D10 - 150 Tul. Memanjang # # D10 - 200 |
| A1 | 150 | Tul. Memendek # # D10 - 100 Tul. Memanjang # # D10 - 150 | A3 | 250 | Tul. Memanjang # # D13 - 150 Tul. Memendek # # D13 - 150 |

Mutu Beton f_c 25 MPa
 Mutu baja ulir (S) f_y : 420 MPa (BJTS 420B)
 Mutu baja polos (P) f_y : 280 MPa (B.JTP.280)



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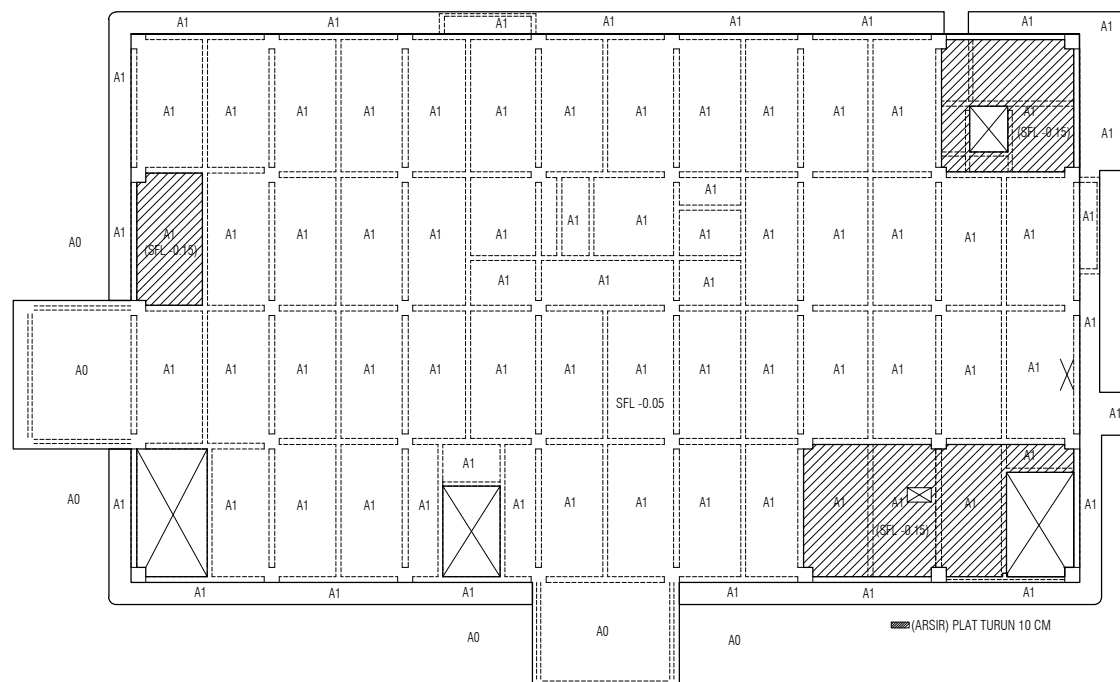
Ranni Sahlinda
 NIM.2019D1B161

KETERANGAN

DENAH PLAT LANTAI 1
 (SFL - 0.05)

JUDUL GAMBAR

| | | |
|---------|------------|-------------|
| SKALA | NO. GAMBAR | JML. GAMBAR |
| 1 : 250 | | |



DENAH PLAT LANTAI 1 (SFL -0.05)

SKALA 1 : 250

LEGENDA GAMBAR

| NOTASI | TEBAL PLAT | TULANGAN | NOTASI | TEBAL PLAT | TULANGAN |
|--------|------------|---|--------|------------|---|
| A0 | 120 | Tul. Wiremesh # # M8 - 150 | A2 | 120 | Tul. Memendek # # D10 - 150 Tul. Memanjang # # D10 - 200 |
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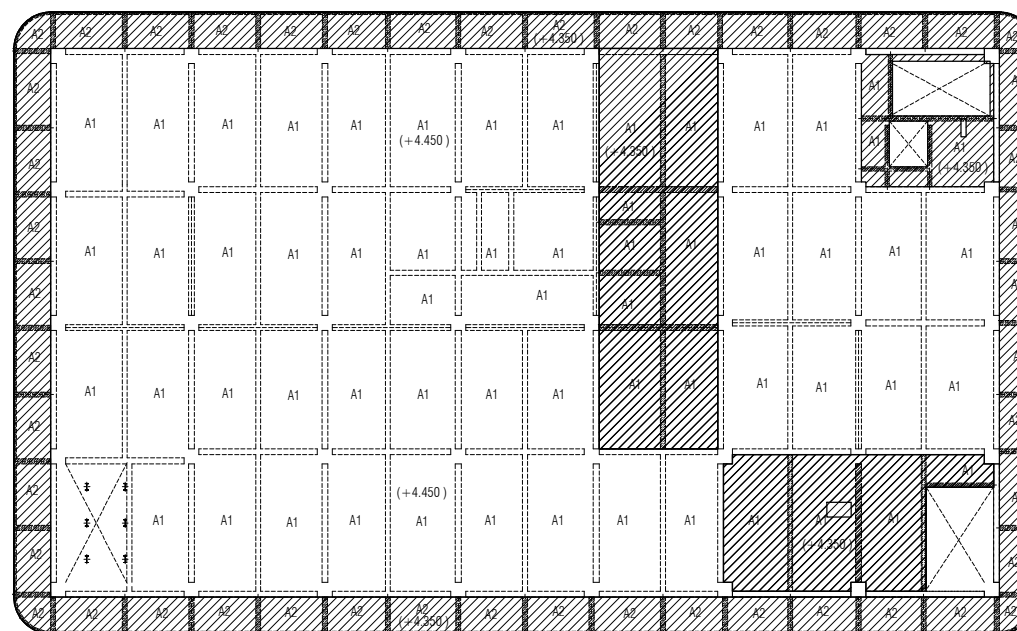
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DENAH PLAT LANTAI 2
 (SFL +4.450)

JUDUL GAMBAR

SKALA NO. GAMBAR JML. GAMBAR

1 : 250



■ (ARSIR) PLAT TURUN 10 CM

DENAH PLAT LANTAI 2 (SFL +4.450)

SKALA 1 : 250

LEGENDA GAMBAR

| NOTASI | TEBAL PLAT | TULANGAN | NOTASI | TEBAL PLAT | TULANGAN |
|--------|------------|---|--------|------------|---|
| A0 | 120 | Tul. Wiremesh # # M8 - 150 | A2 | 120 | Tul. Memendek # # D10 - 150 Tul. Memanjang # # D10 - 200 |
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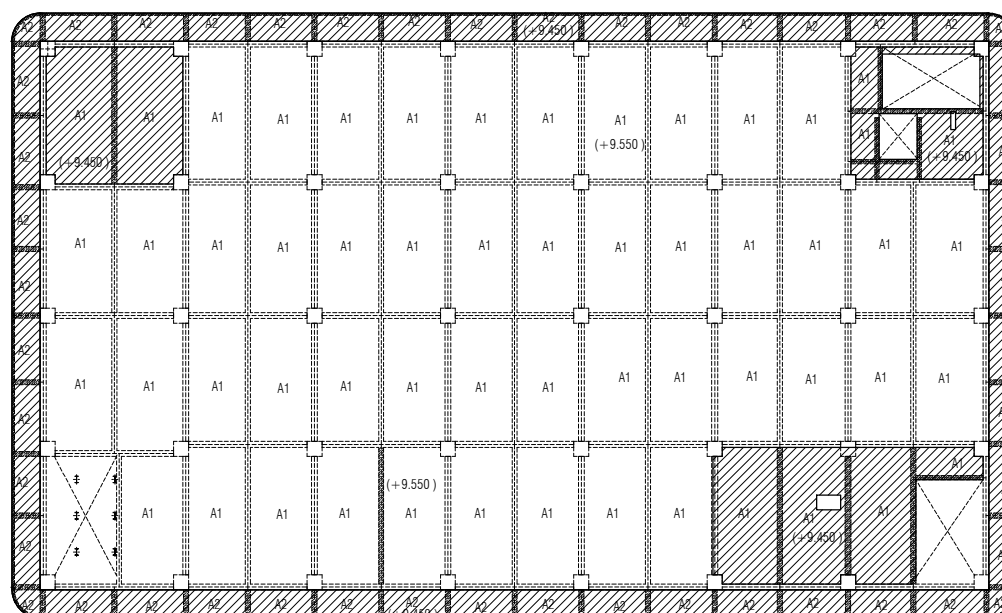
KETERANGAN

DENAH PLAT LANTAI 3
 (SFL +9.550)

JUDUL GAMBAR

SKALA NO. GAMBAR JML. GAMBAR

1 : 250



■ (ARSIR) PLAT TURUN 10 CM

DENAH PLAT LANTAI 3 (SFL +9.550)
 SKALA 1 : 250

LEGENDA GAMBAR

| NOTASI | TEBAL PLAT | TULANGAN | NOTASI | TEBAL PLAT | TULANGAN |
|--------|------------|---|--------|------------|---|
| A0 | 120 | Tul. Wiremesh # # M8 - 150 | A2 | 120 | Tul. Memendek # # D10 - 150 Tul. Memanjang # # D10 - 200 |
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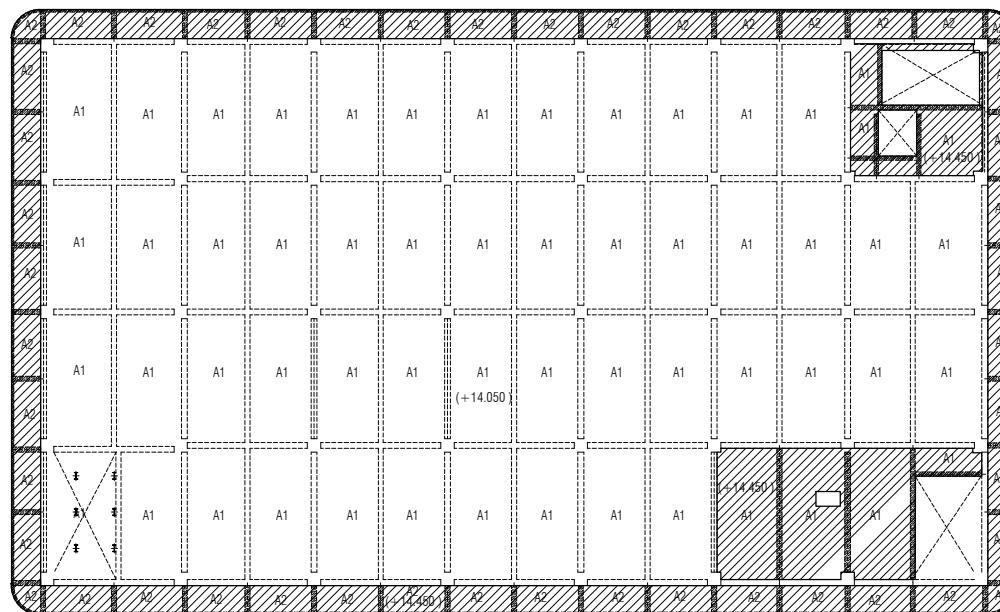
Ranni Sahlinda
 NIM.2019D1B161

KETERANGAN

DENAH PLAT LANTAI 4
 (SFL +14.050)

JUDUL GAMBAR

| | | |
|---------|------------|-------------|
| SKALA | NO. GAMBAR | JML. GAMBAR |
| 1 : 250 | | |



■ (ARSIR) PLAT TURUN 10 CM

DENAH PLAT LANTAI 4 (SFL +14.050)

SKALA 1 : 250

LEGENDA GAMBAR

| NOTASI | TEBAL PLAT | TULANGAN | NOTASI | TEBAL PLAT | TULANGAN |
|--------|------------|---|--------|------------|---|
| A0 | 120 | Tul. Wiremesh # # M8 - 150 | A2 | 120 | Tul. Memendek # # D10 - 150 Tul. Memanjang # # D10 - 200 |
| A1 | 150 | Tul. Memendek # # D10 - 100 Tul. Memanjang # # D10 - 150 | A3 | 250 | Tul. Memanjang # # D13 - 150 Tul. Memendek # # D13 - 150 |

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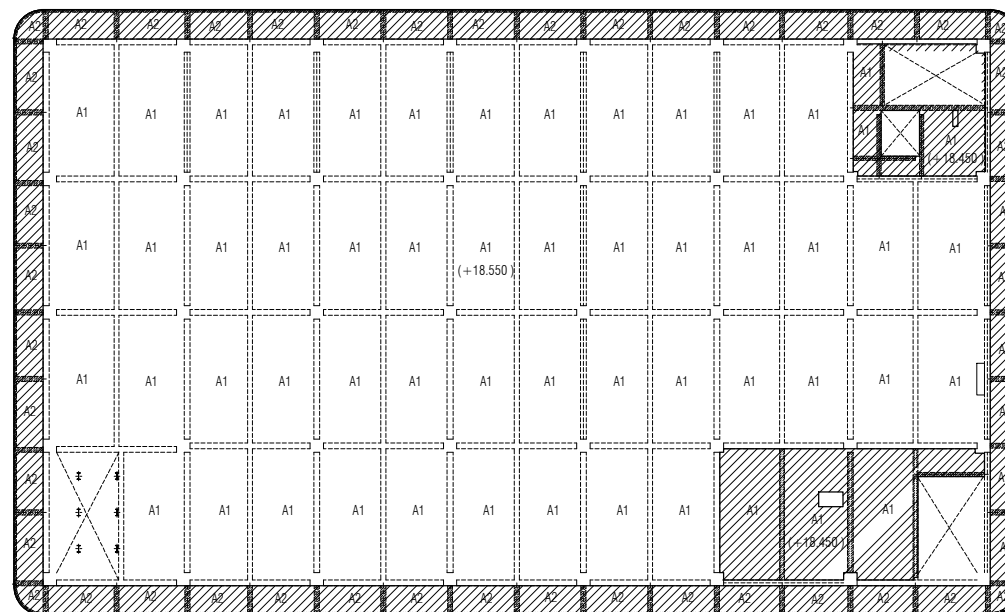
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 NIM.2019D1B161

KETERANGAN

DENAH PLAT LANTAI 5
 (SFL +18.550)

JUDUL GAMBAR

| | | |
|---------|------------|-------------|
| SKALA | NO. GAMBAR | JML. GAMBAR |
| 1 : 250 | | |



■ (ARSIR) PLAT TURUN 10 CM

DENAH PLAT LANTAI 5 (SFL +18.550)

SKALA 1 : 250

LEGENDA GAMBAR

| NOTASI | TEBAL PLAT | TULANGAN | NOTASI | TEBAL PLAT | TULANGAN |
|--------|------------|---|--------|------------|---|
| A0 | 120 | Tul. Wiremesh # # M8 - 150 | A2 | 120 | Tul. Memendek # # D10 - 150 Tul. Memanjang # # D10 - 200 |
| A1 | 150 | Tul. Memendek # # D10 - 100 Tul. Memanjang # # D10 - 150 | A3 | 250 | Tul. Memanjang # # D13 - 150 Tul. Memendek # # D13 - 150 |

Mutu Beton f_c 25 MPa
 Mutu baja ulir (S) f_y : 420 MPa (BJTS 420B)
 Mutu baja polos (P) f_y : 280 MPa (B1TP 280)



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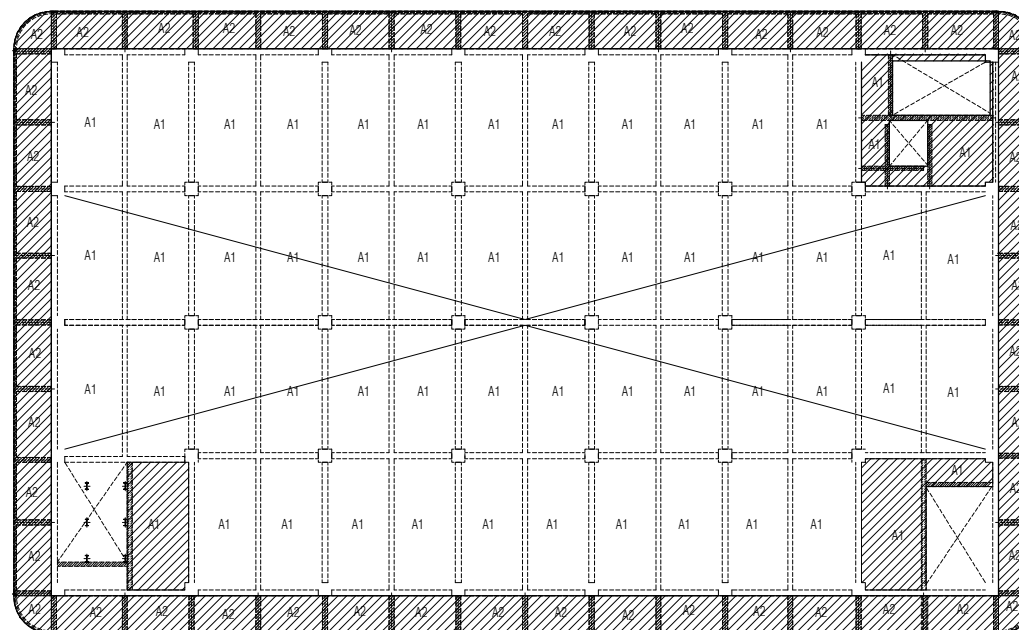
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DENAH PLAT LANTAI ATAP
 (SFL +23.050)

JUDUL GAMBAR

SKALA NO. GAMBAR JML. GAMBAR

1 : 300



DENAH PLAT LANTAI ATAP (SFL +23.050)

SKALA 1 : 300

LEGENDA GAMBAR

| NOTASI | TEBAL PLAT | TULANGAN | NOTASI | TEBAL PLAT | TULANGAN |
|--------|------------|---|--------|------------|---|
| A0 | 120 | Tul. Wiremesh # # M8 - 150 | A2 | 120 | Tul. Memendek # # D10 - 150 Tul. Memanjang # # D10 - 200 |
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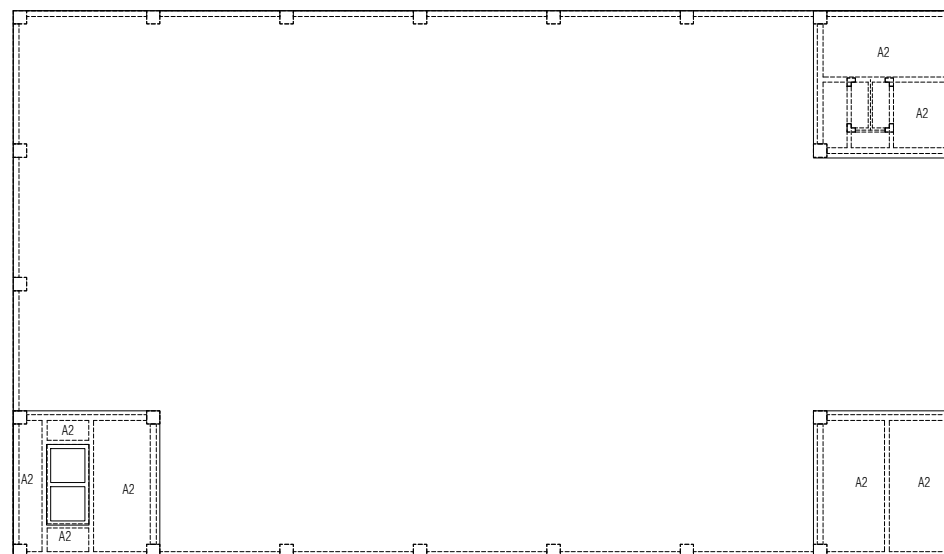
KETERANGAN

DENAH PLAT LANTAI ATAP
 (SFL +27.550)

JUDUL GAMBAR

SKALA NO. GAMBAR JML. GAMBAR

1 : 300



DENAH PLAT LANTAI ATAP (SFL +27.550)

SKALA 1 : 300

LEGENDA GAMBAR

| NOTASI | TEBAL PLAT | TULANGAN | NOTASI | TEBAL PLAT | TULANGAN |
|--------|------------|---|--------|------------|---|
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| A1 | 150 | Tul. Memendek # # D10 - 100 Tul. Memanjang # # D10 - 150 | A3 | 250 | Tul. Memanjang # # D13 - 150 Tul. Memendek # # D13 - 150 |

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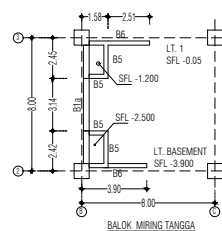
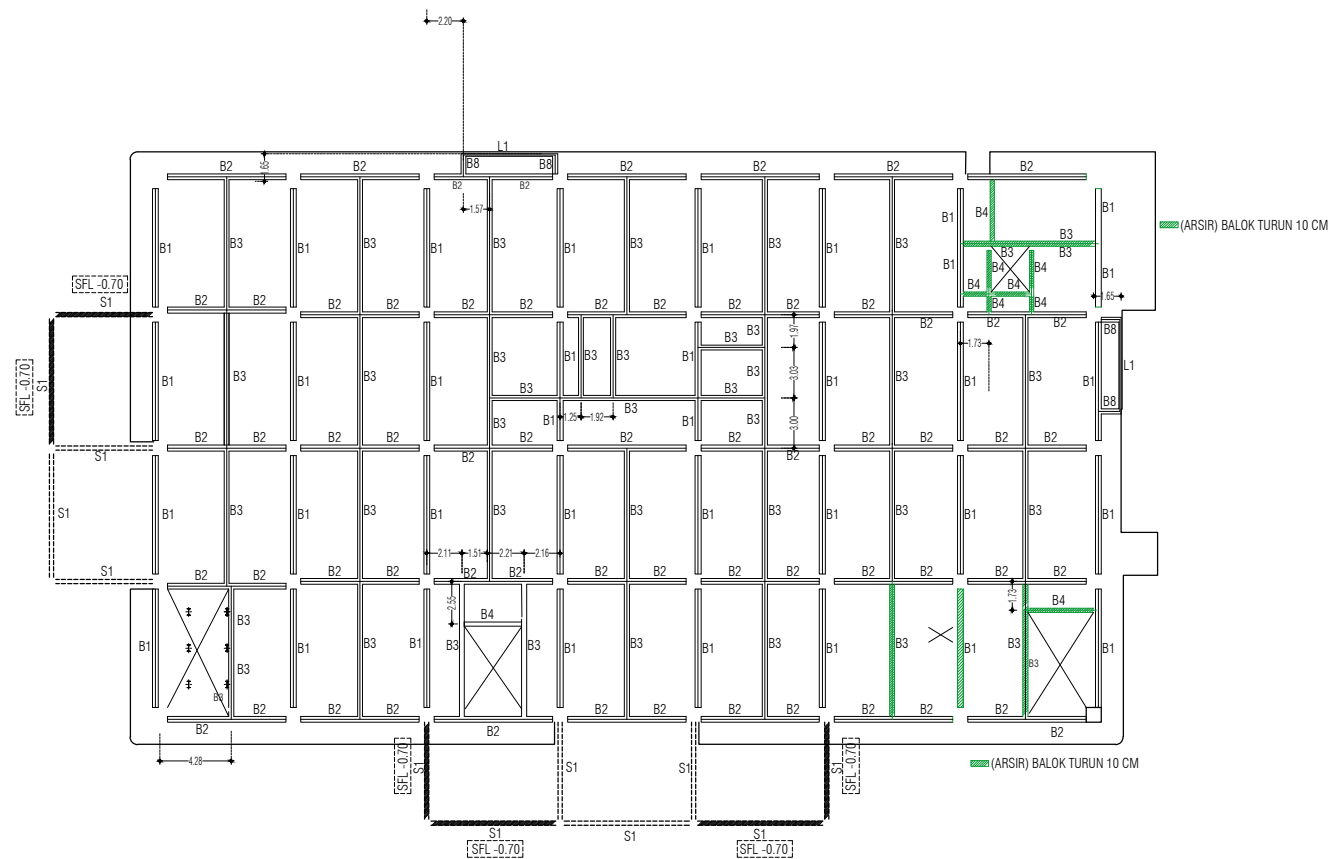
DENAH BALOK LANTAI 1
(SFL - 0.05)

JUDUL GAMBAR

LEGENDA GAMBAR

| NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN |
|--------|------------------------|--------|------------------------|--------|-----------------------|--------|------------------------|
| K5 | Kolom K5 - 500x500 mm | B2 | Balok B2 - 350x700 mm | B5 | Balok B5 - 250x500 mm | B10 | Balok B10 - 350x700 mm |
| B1 | Balok B1 - 350x700 mm | B2a | Balok B2a - 350x700 mm | B6 | Balok B6 - 250x500 mm | B11 | Balok B11 - 300x700 mm |
| B1a | Balok B1a - 350x700 mm | B3 | Balok B3 - 300x600 mm | B7 | Balok B7 - 250x500 mm | L1 | Balok L1 - 150x600 mm |
| B1b | Balok B1b - 350x700 mm | B3a | Balok B3a - 300x600 mm | B8 | Balok B8 - 300x600 mm | L2 | Balok L2 - 150x700 mm |
| B1c | Balok B1c - 350x850 mm | B4 | Balok B4 - 250x400 mm | B9 | Balok B9 - 300x600 mm | | |

Mutu Beton f'c 25 MPa
Mutu Baja BJ-37
Mutu baja ulir (S) fy : 420 MPa (BJTS 420B)
Mutu baja polos (P) fy : 280 MPa (BJTP 280)



DENAH BALOK LANTAI 1 (SFL -0.05)

SKALA 1 : 250

1 : 250

SKALA NO. GAMBAR JML. GAMBAR



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NIM.2019D1B161

KETERANGAN

DENAH BALOK LANTAI 2
(SFL + 4.450)

JUDUL GAMBAR

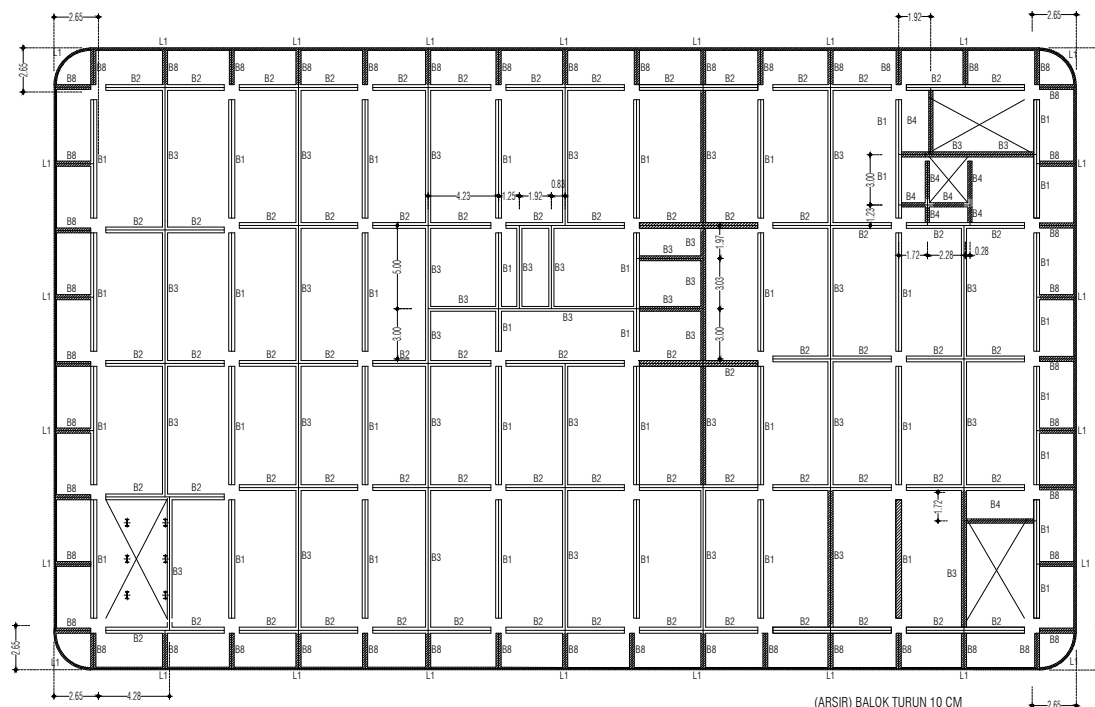
LEGENDA GAMBAR

| NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN |
|--------|------------------------|--------|------------------------|--------|-----------------------|--------|------------------------|
| K5 | Kolom K5 - 500x500 mm | B2 | Balok B2 - 350x700 mm | B5 | Balok B5 - 250x500 mm | B10 | Balok B10 - 350x700 mm |
| B1 | Balok B1 - 350x700 mm | B2a | Balok B2a - 350x700 mm | B6 | Balok B6 - 250x500 mm | B11 | Balok B11 - 300x700 mm |
| B1a | Balok B1a - 350x700 mm | B3 | Balok B3 - 300x600 mm | B7 | Balok B7 - 250x500 mm | L1 | Balok L1 - 150x600 mm |
| B1b | Balok B1b - 350x700 mm | B3a | Balok B3a - 300x600 mm | B8 | Balok B8 - 300x600 mm | L2 | Balok L2 - 150x700 mm |
| B1c | Balok B1c - 350x850 mm | B4 | Balok B4 - 250x400 mm | B9 | Balok B9 - 300x600 mm | | |

Mutu Beton f_c 25 MPa
Mutu Baja BJ-37
Mutu baja ulir (S) f_y : 420 MPa (BJTS 420B)
Mutu baja polos (P) f_y : 280 MPa (BJTP 280)

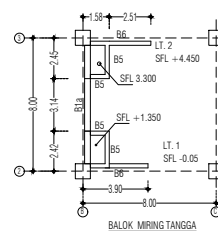
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DENAH BALOK LANTAI 2 (SFL + 4.450)

SKALA 1 : 250





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KETERANGAN

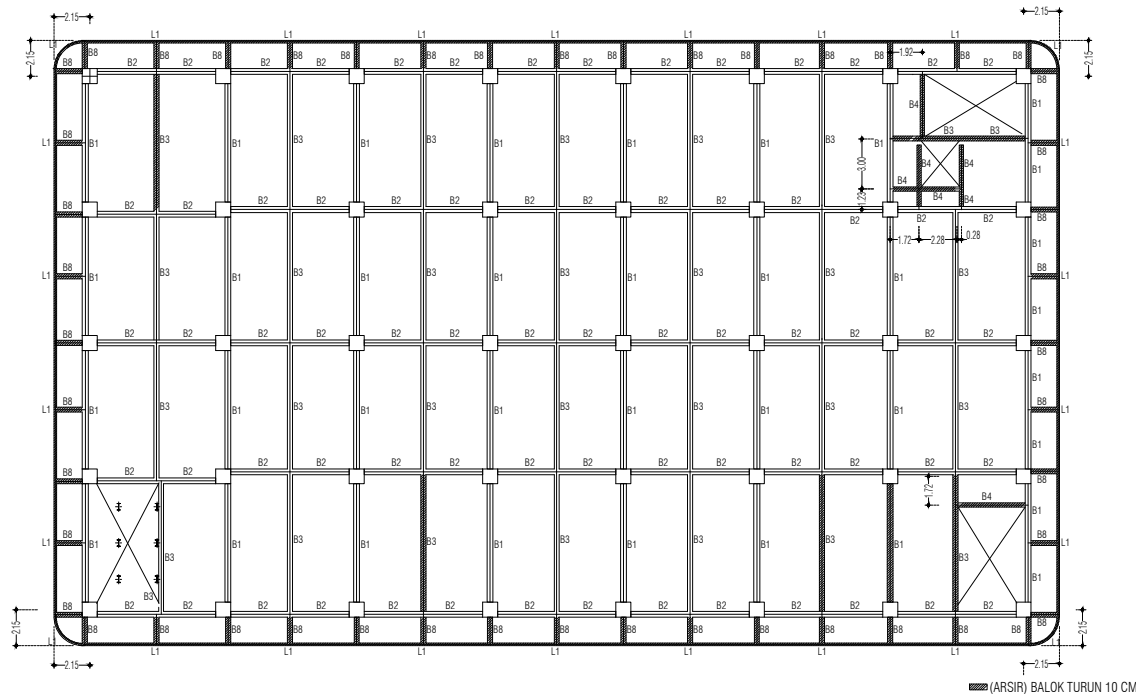
DENAH BALOK LANTAI 3
(SFL +9.550)

JUDUL GAMBAR

LEGENDA GAMBAR

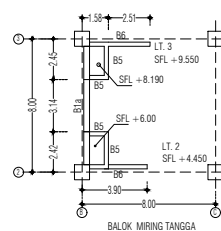
| NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN |
|--------|------------------------|--------|------------------------|--------|-----------------------|--------|------------------------|
| K5 | Kolom K5 - 500x500 mm | B2 | Balok B2 - 350x700 mm | B5 | Balok B5 - 250x500 mm | B10 | Balok B10 - 350x700 mm |
| B1 | Balok B1 - 350x700 mm | B2a | Balok B2a - 350x700 mm | B6 | Balok B6 - 250x500 mm | B11 | Balok B11 - 300x700 mm |
| B1a | Balok B1a - 350x700 mm | B3 | Balok B3 - 300x600 mm | B7 | Balok B7 - 250x500 mm | L1 | Balok L1 - 150x600 mm |
| B1b | Balok B1b - 350x700 mm | B3a | Balok B3a - 300x600 mm | B8 | Balok B8 - 300x600 mm | L2 | Balok L2 - 150x700 mm |
| B1c | Balok B1c - 350x850 mm | B4 | Balok B4 - 250x400 mm | B9 | Balok B9 - 300x600 mm | | |

Mutu Beton f'c 25 MPa
Mutu Baja BJ-37
Mutu baja ulir (S) fy : 420 MPa (BJTS 420B)
Mutu baja polos (P) fy : 280 MPa (BJTP 280)



DENAH BALOK LANTAI 3 (SFL +9.550)

SKALA 1 : 250



SKALA

NO. GAMBAR

JML. GAMBAR

1 : 250



UNIVERSITAS MUHAMMADIYAH MATARAM
FAKULTAS TEKNIK
PROGRAM STUDI TEKNIK

JUDUL TUGAS AKHIR

Pengaruh Penempatan Dinding Geser Terhadap
Perilaku Struktur Gedung Bank NTB Syariah
Mataram

DOSEN PEMBIMBING

Pembimbing I

Dr.Eng. Hariyadi,ST., M.Sc (Eng)
NIDN.0027107301

Pembimbing II

Ahmad Zarkasi, ST., MT.
NIDN.0819068903

NAMA MAHASISWA

Ranni Sahlinda
NIM.2019D1B161

KETERANGAN

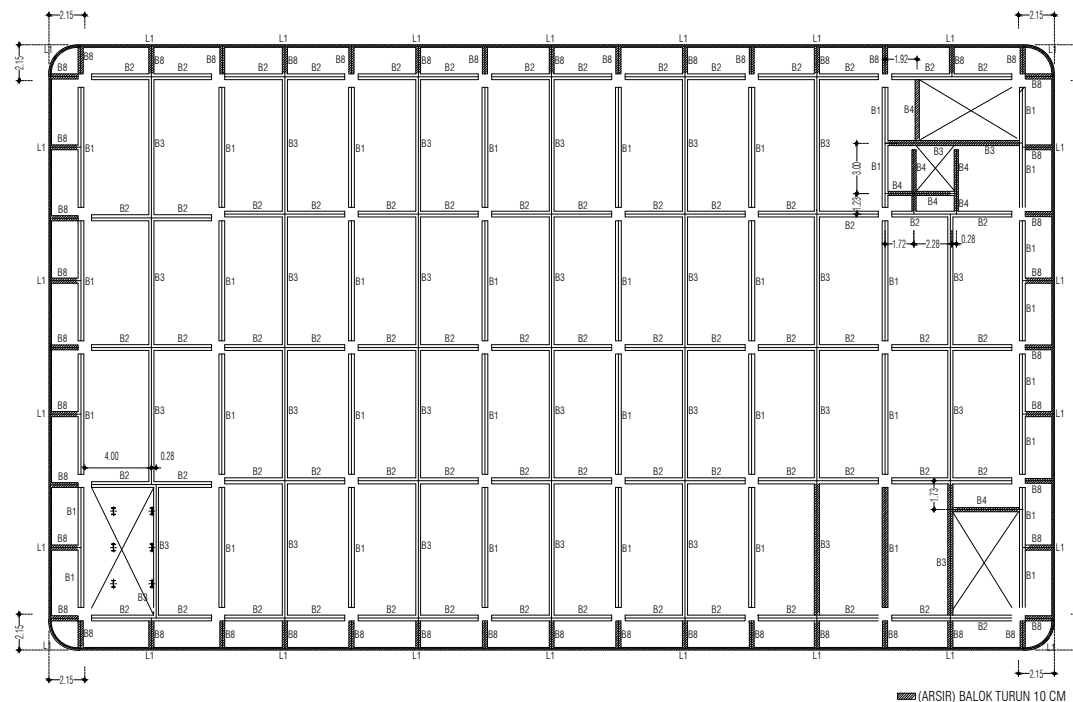
DENAH BALOK LANTAI 4
(SFL +14.550)

JUDUL GAMBAR

LEGENDA GAMBAR

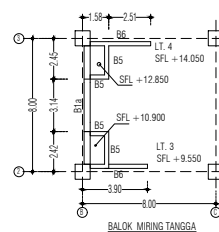
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|--------|------------------------|--------|------------------------|--------|-----------------------|--------|------------------------|
| K5 | Kolom K5 - 500x500 mm | B2 | Balok B2 - 350x700 mm | B5 | Balok B5 - 250x500 mm | B10 | Balok B10 - 350x700 mm |
| B1 | Balok B1 - 350x700 mm | B2a | Balok B2a - 350x700 mm | B6 | Balok B6 - 250x500 mm | B11 | Balok B11 - 300x700 mm |
| B1a | Balok B1a - 350x700 mm | B3 | Balok B3 - 300x600 mm | B7 | Balok B7 - 250x500 mm | L1 | Balok L1 - 150x600 mm |
| B1b | Balok B1b - 350x700 mm | B3a | Balok B3a - 300x600 mm | B8 | Balok B8 - 300x600 mm | L2 | Balok L2 - 150x700 mm |
| B1c | Balok B1c - 350x850 mm | B4 | Balok B4 - 250x400 mm | B9 | Balok B9 - 300x600 mm | | |

Mutu Beton f_c 25 MPa
Mutu Baja BJ-37
Mutu baja ulir (S) f_y: 420 MPa (BJTS 420B)
Mutu baja polos (P) f_y: 280 MPa (BJTP 280)



DENAH BALOK LANTAI 4 (SFL +14.050)

SKALA 1 : 250



1 : 250

SKALA NO. GAMBAR JML. GAMBAR



UNIVERSITAS MUHAMMADIYAH MATARAM
FAKULTAS TEKNIK
PROGRAM STUDI TEKNIK

JUDUL TUGAS AKHIR

Pengaruh Penempatan Dinding Geser Terhadap
Perilaku Struktur Gedung Bank NTB Syariah
Mataram

DOSEN PEMBIMBING

Pembimbing I

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Ahmad Zarkasi, ST., MT.
NIDN.0819068903

NAMA MAHASISWA

Ranni Sahlinda
NIM.2019D1B161

KETERANGAN

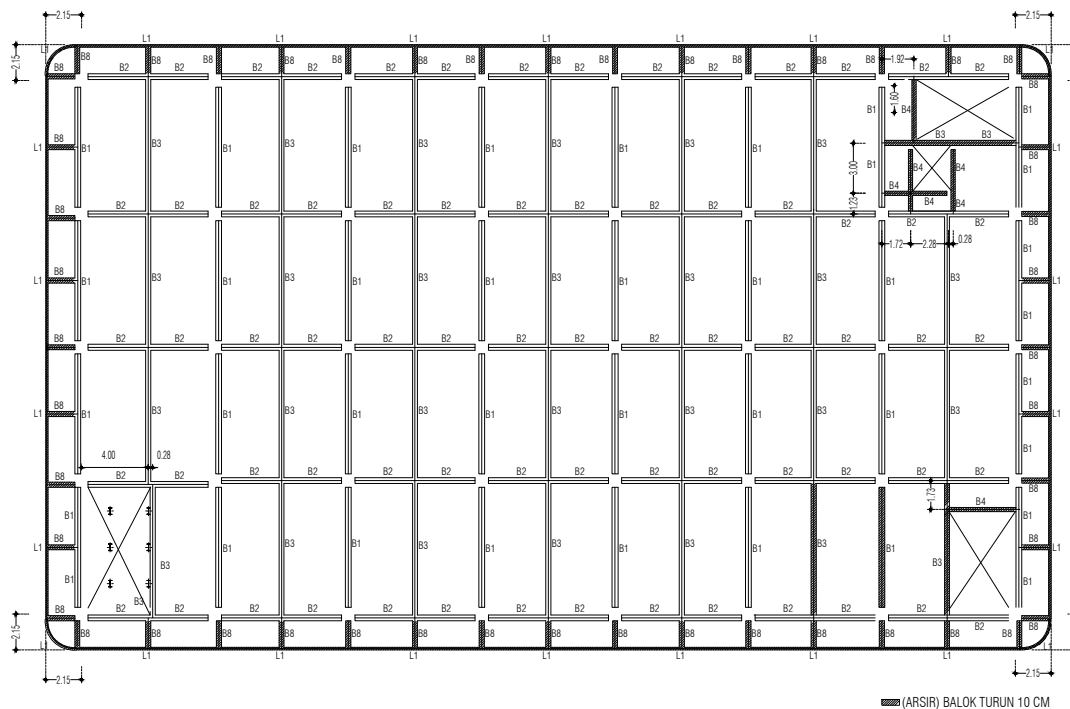
DENAH BALOK LANTAI 5
(SFL +18.550)

JUDUL GAMBAR

LEGENDA GAMBAR

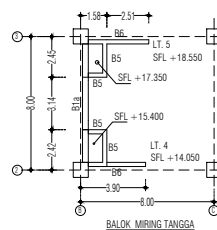
| NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN |
|--------|------------------------|--------|------------------------|--------|-----------------------|--------|------------------------|
| K5 | Kolom K5 - 500x500 mm | B2 | Balok B2 - 350x700 mm | B5 | Balok B5 - 250x500 mm | B10 | Balok B10 - 350x700 mm |
| B1 | Balok B1 - 350x700 mm | B2a | Balok B2a - 350x700 mm | B6 | Balok B6 - 250x500 mm | B11 | Balok B11 - 300x700 mm |
| B1a | Balok B1a - 350x700 mm | B3 | Balok B3 - 300x600 mm | B7 | Balok B7 - 250x500 mm | L1 | Balok L1 - 150x600 mm |
| B1b | Balok B1b - 350x700 mm | B3a | Balok B3a - 300x600 mm | B8 | Balok B8 - 300x600 mm | L2 | Balok L2 - 150x700 mm |
| B1c | Balok B1c - 350x850 mm | B4 | Balok B4 - 250x400 mm | B9 | Balok B9 - 300x600 mm | | |

Mutu Beton f'c : 25 MPa
Mutu Baja BJ-37
Mutu baja ulir (S) fy : 420 MPa (BJTS 420B)
Mutu baja polos (P) fy : 280 MPa (BJTP 280)



DENAH BALOK LANTAI 5 (SFL +18.550)

SKALA 1 : 250



BALOK MIRING TANGGA

1 : 250

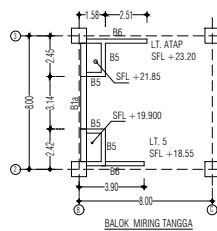
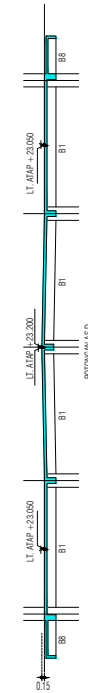
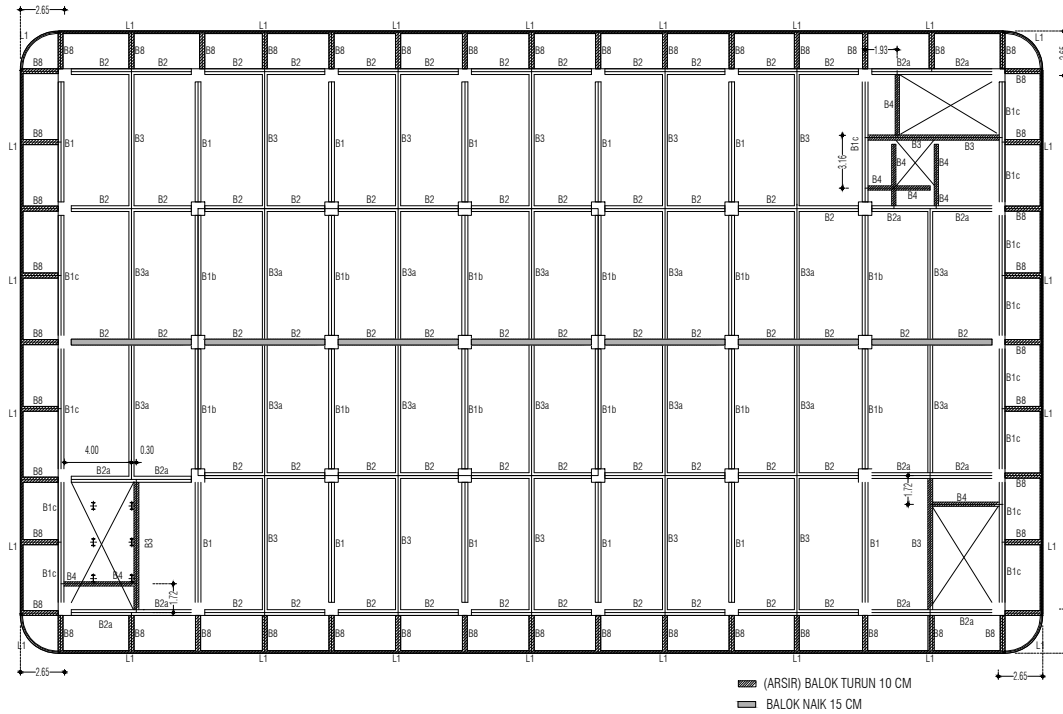
SKALA NO. GAMBAR JML. GAMBAR



LEGENDA GAMBAR

| NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN |
|--------|------------------------|--------|------------------------|--------|-----------------------|--------|------------------------|
| K5 | Kolom K5 - 500x500 mm | B2 | Balok B2 - 350x700 mm | B5 | Balok B5 - 250x500 mm | B10 | Balok B10 - 350x700 mm |
| B1 | Balok B1 - 350x700 mm | B2a | Balok B2a - 350x700 mm | B6 | Balok B6 - 250x500 mm | B11 | Balok B11 - 300x700 mm |
| B1a | Balok B1a - 350x700 mm | B3 | Balok B3 - 300x600 mm | B7 | Balok B7 - 250x500 mm | L1 | Balok L1 - 150x600 mm |
| B1b | Balok B1b - 350x700 mm | B3a | Balok B3a - 300x600 mm | B8 | Balok B8 - 300x600 mm | L2 | Balok L2 - 150x700 mm |
| B1c | Balok B1c - 350x850 mm | B4 | Balok B4 - 250x400 mm | B9 | Balok B9 - 300x600 mm | | |

Mutu Beton: f_c 25 MPa
 Mutu Baja BJ-37
 Mutu baja ulir (S) f_y : 420 MPa (BJTS 420B)
 Mutu baja polos (P) f_y : 280 MPa (BJTP 280)



DENAH BALOK LANTAI ATAP (SFL + 23.050)
 SKALA 1 : 250

| SKALA | NO. GAMBAR | JML. GAMBAR |
|---------|------------|-------------|
| 1 : 250 | | |



UNIVERSITAS MUHAMMADIYAH MATARAM
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JUDUL TUGAS AKHIR

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Ranni Sahlinda
 NIM.2019D1B161

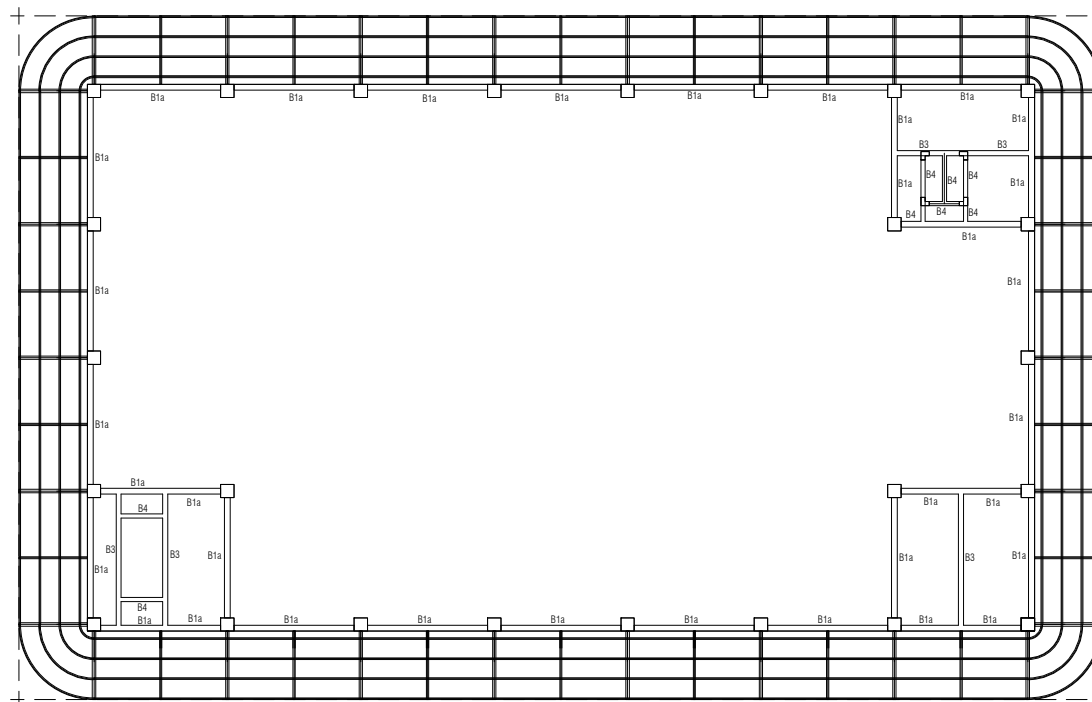
KETERANGAN

DENAH BALOK LANTAI ATAP
 (SFL +27.550)

JUDUL GAMBAR

SKALA NO. GAMBAR JML. GAMBAR

1 : 250



DENAH BALOK LANTAI ATAP (SFL +27.550)

SKALA 1 : 250

LEGENDA GAMBAR

| NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN | NOTASI | KETERANGAN |
|--------|------------------------|--------|------------------------|--------|-----------------------|--------|------------------------|
| K5 | Kolom K5 - 500x500 mm | B2 | Balok B2 - 350x700 mm | B5 | Balok B5 - 250x500 mm | B10 | Balok B10 - 350x700 mm |
| B1 | Balok B1 - 350x700 mm | B2a | Balok B2a - 350x700 mm | B6 | Balok B6 - 250x500 mm | B11 | Balok B11 - 300x700 mm |
| B1a | Balok B1a - 350x700 mm | B3 | Balok B3 - 300x600 mm | B7 | Balok B7 - 250x500 mm | L1 | Balok L1 - 150x600 mm |
| B1b | Balok B1b - 350x700 mm | B3a | Balok B3a - 300x600 mm | B8 | Balok B8 - 300x600 mm | L2 | Balok L2 - 150x700 mm |
| B1c | Balok B1c - 350x850 mm | B4 | Balok B4 - 250x400 mm | B9 | Balok B9 - 300x600 mm | | |

Mutu Beton f'c 25 MPa
 Mutu Baja BJ-37
 Mutu baja ulir (S) fy : 420 MPa (BJTS 420B)
 Mutu baja polos (P) fy : 280 MPa (BJTP 280)



UNIVERSITAS MUHAMMADIYAH MATARAM
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Ranni Sahlinda
 NIM.2019D1B161

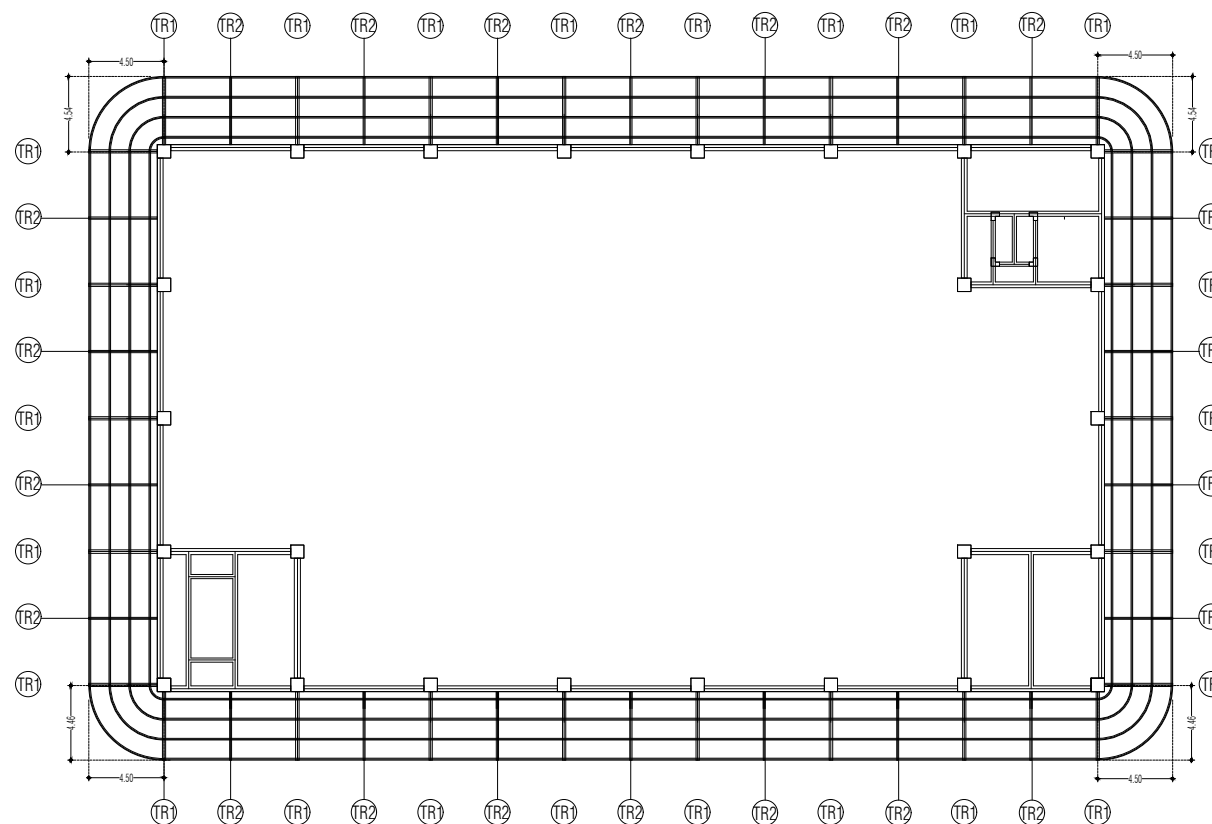
KETERANGAN

DENAH RANGKA TRITISAN
 LANTAI ATAP
 (SFL +27.550)

JUDUL GAMBAR

| SKALA | NO. GAMBAR | JML. GAMBAR |
|-------|------------|-------------|
|-------|------------|-------------|

| | | |
|---------|--|--|
| 1 : 300 | | |
|---------|--|--|



DENAH RANGKA TRITISAN LANTAI ATAP (SFL +27.550)
 SKALA 1 : 300



UNIVERSITAS MUHAMMADIYAH MATARAM
 FAKULTAS TEKNIK
 PROGRAM STUDI TEKNIK

JUDUL TUGAS AKHIR

Pengaruh Penempatan Dinding Geser Terhadap
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NAMA MAHASISWA

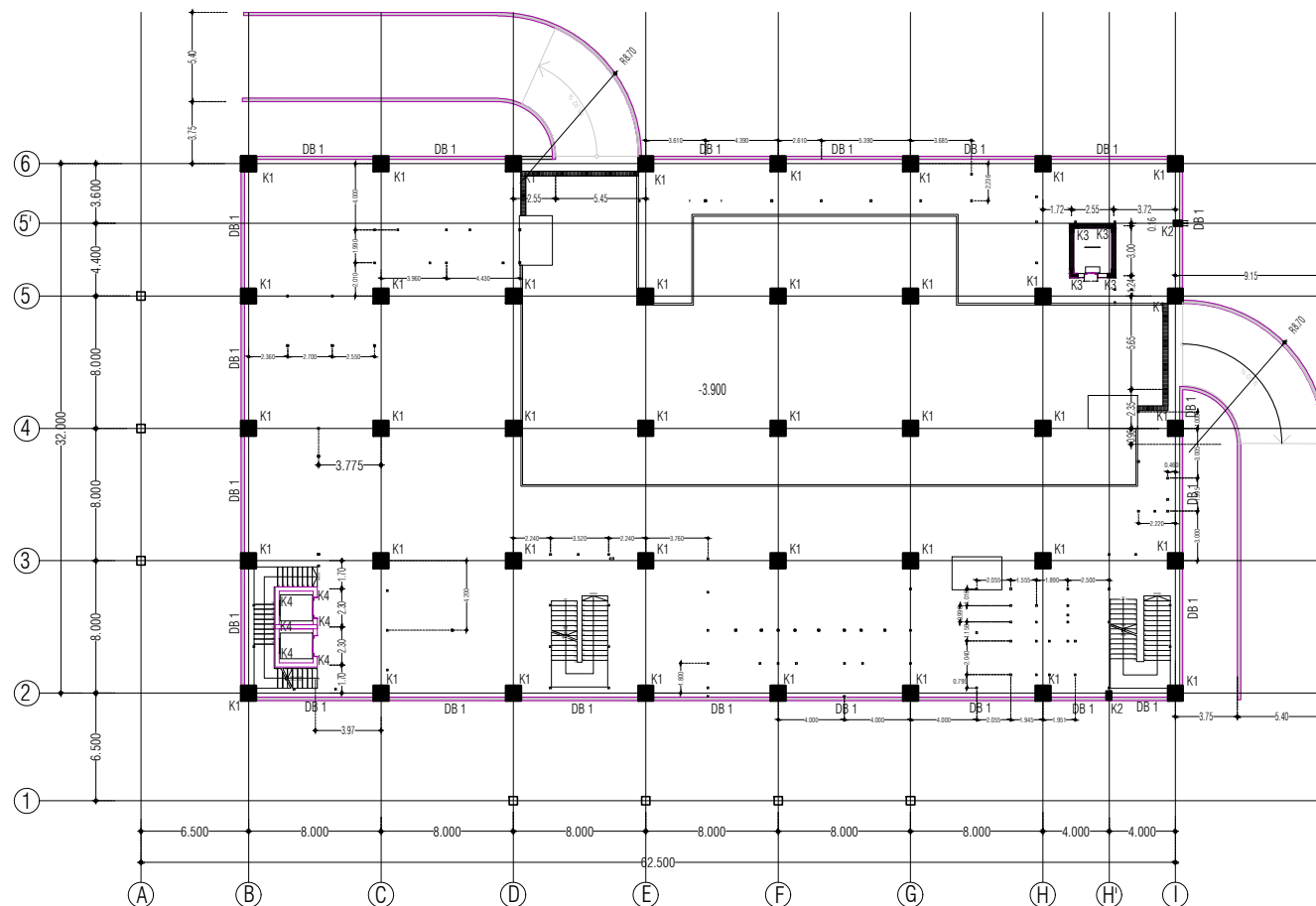
Ranni Sahlinda
 NIM.2019D1B161

KETERANGAN

DENAH KOLOM LANTAI BASEMENT
 (SFL - 3.900)

JUDUL GAMBAR

| | | |
|---------|------------|-------------|
| SKALA | NO. GAMBAR | JML. GAMBAR |
| 1 : 300 | | |



DENAH KOLOM LANTAI BASEMENT (SFL -3.900)

SKALA 1 : 300

LEGENDA GAMBAR

| NO | NOTASI | KETERANGAN | NO | NOTASI | KETERANGAN |
|----|--------|--------------------------------|----|--------|--------------------------------|
| 01 | K1 | Kolom K1 - 900x900 mm | 06 | K5 | Kolom K5 - 500x500 mm |
| 02 | K1a | Kolom K1a - 800x800 mm | 07 | S1 | Balok S1 - 300x500 mm |
| 03 | K2 | Kolom K2 - 300x500 mm | 08 | S2 | Balok S2 - 250x400 mm |
| 04 | K3 | Kolom K3 - 250x250x500 mm | 09 | DB1 | Dinding Beton DB1 tebal 200 mm |
| 05 | K4 | Kolom K4 - IWF 400x200x8x13 mm | 10 | DB2 | Dinding Beton DB2 tebal 200 mm |

Mutu Beton fc 25 MPa
 Mutu Baja BJ-37
 Mutu baja ulir (S) fy : 420 MPa (BJTS 420B)
 Mutu baja polos (P) fy : 280 MPa (BJTP 280)



Laporan Pendahuluan SOIL TEST

November 2020



Proyek :

Soil Test PERENCANAAN PEMBANGUNAN GEDUNG BANK NTB

Kota Mataram- Nusa Tenggara Barat

46/ LAPORAN / GEOTEKNIK / XI / 2020





LABORATORIUM GEOTEKNIK DAN MEKANIKA TANAH

Kementerian Riset, Teknologi Dan Pendidikan Tinggi

FAKULTAS TEKNIK UNIVERSITAS MATARAM

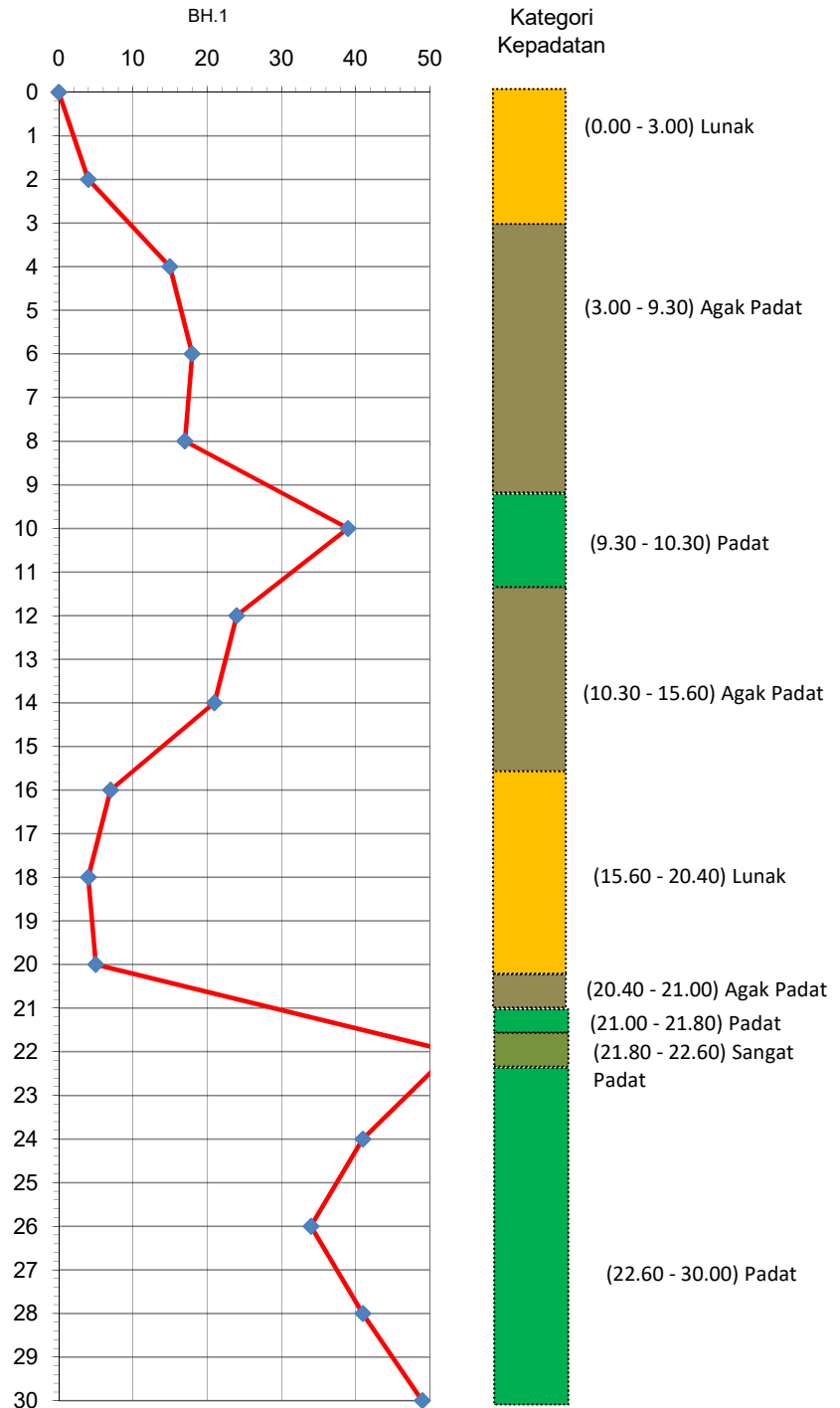
Jalan Majapahit No. 62 Tlp. 0370 7502698 e-mail: geoteknik2017@gmail.com

PROYEK

SOIL TEST PERENCANAAN GEDUNG DAN BANGUNAN BANK NTB

| | |
|-----------------|------------------------------|
| NOMOR LAPORAN | SOILTEST - 46.XI. 2020 - MCS |
| LOKASI | Kota Mataram - NTB |
| NAMA LUBANG BOR | BH.1 |
| KOORDINAT | MAT : - m |

| Kedalaman | 15 cm (1) | 15 cm (2) | 15 cm (3) | N- SPT |
|-----------|-----------|-----------|-----------|--------|
| 0 | | | | 0 |
| 2 | 2 | 2 | 2 | 4 |
| 4 | 6 | 7 | 8 | 15 |
| 6 | 7 | 9 | 9 | 18 |
| 8 | 7 | 8 | 9 | 17 |
| 10 | 15 | 17 | 22 | 39 |
| 12 | 8 | 9 | 15 | 24 |
| 14 | 9 | 7 | 14 | 21 |
| 16 | 4 | 3 | 4 | 7 |
| 18 | 2 | 2 | 2 | 4 |
| 20 | 2 | 2 | 3 | 5 |
| 22 | 19 | 21 | 32 | 53 |
| 24 | 17 | 19 | 22 | 41 |
| 26 | 11 | 15 | 19 | 34 |
| 28 | 13 | 16 | 25 | 41 |
| 30 | 13 | 20 | 29 | 49 |



ANALISA DAYA DUKUNG

| | |
|----------------|--|
| Nomor Laporan | : SOILTEST - 46.XI. 2020 - MCS |
| Nama Pekerjaan | : SOIL TEST PERENCANAAN GEDUNG DAN BANGUNAN BANK NTB |
| Lokasi | : Kota Mataram - NTB |
| Titik Bor | : BH . 1 |
| Koordinat | : - - |
| Jenis Analisa | : Pondasi Dangkal |
| Metode | : Meyerhof |

Data Lapangan (SPT)

| Kedalaman (m) | Nilia SPT (puulan) |
|--------------------|-------------------------|
| 0.00 | 0 |
| 2.00 | 4 |
| 4.00 | 15 |
| 6.00 | 18 |
| 8.00 | 17 |
| 10.00 | 39 |
| 12.00 | 24 |
| 14.00 | 21 |
| 16.00 | 7 |
| 18.00 | 4 |
| 20.00 | 5 |
| 22.00 | 53 |
| 24.00 | 41 |
| 26.00 | 34 |
| 28.00 | 41 |
| 30.00 | 49 |

A. Nilai rata - rata SPT (N50)

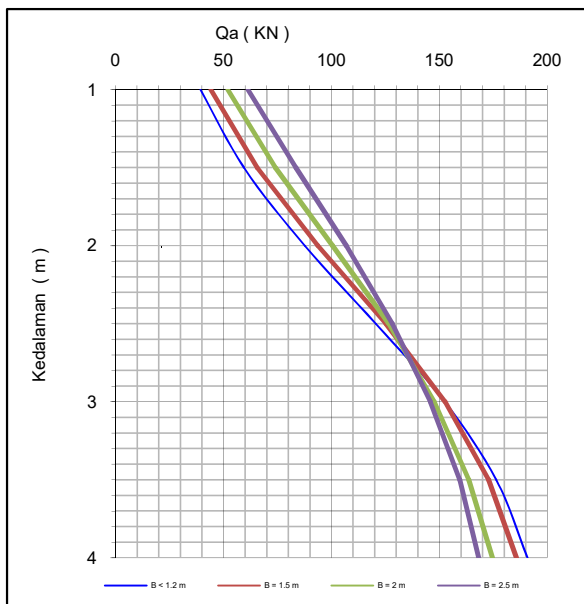
| Kedalaman Pondasi (m) | Jenis Tanah | Lebar Pondasi (B) dalam m' | | | |
|----------------------------|-----------------|------------------------------|------|------|------|
| | | < 1.2 | 1.50 | 2.00 | 2.50 |
| 1.00 | Lanau Kepasiran | 3 | 4 | 5 | 6 |
| 1.50 | | 5 | 6 | 7 | 8 |
| 2.00 | | 7 | 8 | 10 | 11 |
| 2.50 | Pasir Kelanauan | 10 | 11 | 12 | 13 |
| 3.00 | | 13 | 13 | 14 | 15 |
| 3.50 | | 15 | 15 | 15 | 16 |
| 4.00 | | 16 | 16 | 17 | 17 |

B. Kapasitas Dukung Tanah (q_a)

| Kedalaman Pondasi (m) | Kapasitas Dukung Tanah (q _a) KN/m ² | | | |
|----------------------------|---|-----------|---------|-----------|
| | B < 1.2 m | B = 1.5 m | B = 2 m | B = 2.5 m |
| 1.00 | 39 | 44 | 52 | 61 |
| 1.50 | 59 | 66 | 74 | 84 |
| 2.00 | 88 | 94 | 101 | 107 |
| 2.50 | 121 | 125 | 127 | 128 |
| 3.00 | 152 | 153 | 148 | 146 |
| 3.50 | 176 | 173 | 164 | 160 |
| 4.00 | 191 | 186 | 175 | 168 |

Penanggung Jawab Lap :

B. Grafik Daya Dukung Ijin Tanah Pondasi Dangkal



Masyhari

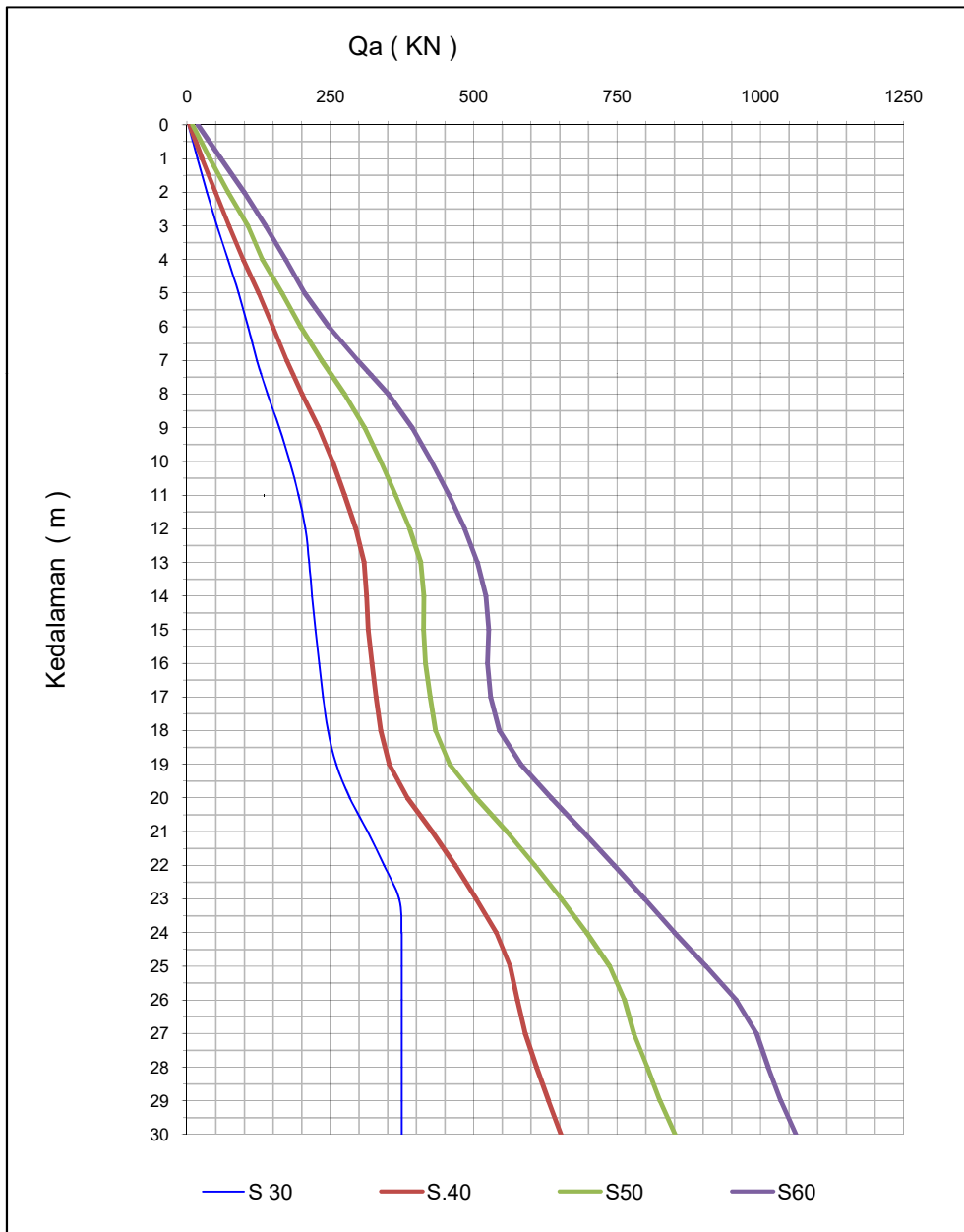
Diperiksa :

Mr.Ikhwan, ST

ANALISA DAYA DUKUNG

| | |
|-----------------------|--|
| Nomor Laporan | : SOILTEST - 46.XI. 2020 - MCS |
| Nama Pekerjaan | : SOIL TEST PERENCANAAN GEDUNG DAN BANGUNAN BANK NTB |
| Lokasi | : Kota Mataram - NTB |
| Titik Bor | : BH . 1 |
| Koordinat | : - - - Elevasi : - |
| Jenis Analisa | : Pondasi Pile |
| Metode | : Meyerhof |
| Data Lapangan (SPT) | Nilai SPT |

B. Grafik Daya Dukung Ijin Tanah Pondasi Dalam (Pile)





LABORATORIUM GEOTEKNIK DAN MEKANIKA TANAH

Kementrian Riset, Teknologi Dan Pendidikan Tinggi

FAKULTAS TEKNIK UNIVERSITAS MATARAM

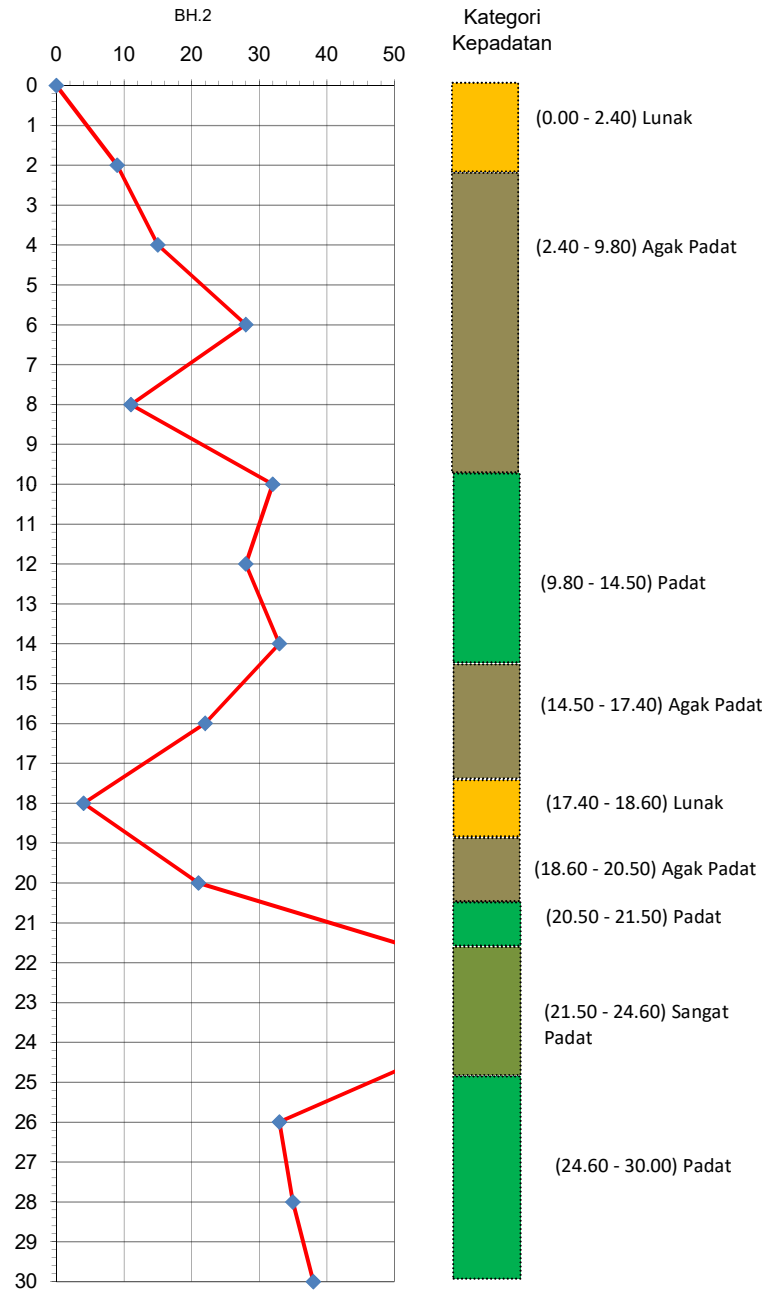
Jalan Majapahit No.62 Tlp. 0370 7502698 e-mail: geoteknik2017@gmail.com

PROYEK

SOIL TEST PERENCANAAN GEDUNG DAN BANGUNAN BANK NTB

| | | | |
|-----------------|------------------------------|--|--|
| NOMOR LAPORAN | SOILTEST - 46.XI. 2020 - MCS | | |
| LOKASI | Kota Mataram - NTB | | |
| NAMA LUBANG BOR | BH.2 | | |
| KOORDINAT | MAT : - m | | |

| Kedalaman | 15 cm (1) | 15 cm (2) | 15 cm (3) | N- SPT |
|-----------|-----------|-----------|-----------|--------|
| 0 | | | | 0 |
| 2 | 5 | 4 | 5 | 9 |
| 4 | 3 | 6 | 9 | 15 |
| 6 | 9 | 13 | 15 | 28 |
| 8 | 4 | 5 | 6 | 11 |
| 10 | 11 | 15 | 17 | 32 |
| 12 | 9 | 12 | 16 | 28 |
| 14 | 11 | 15 | 18 | 33 |
| 16 | 2 | 3 | 19 | 22 |
| 18 | 2 | 2 | 2 | 4 |
| 20 | 17 | 11 | 10 | 21 |
| 22 | 50/5 | - | - | > 50 |
| 24 | 50/5 | - | - | > 50 |
| 26 | 9 | 15 | 18 | 33 |
| 28 | 8 | 16 | 19 | 35 |
| 30 | 10 | 17 | 21 | 38 |



ANALISA DAYA DUKUNG

| | |
|----------------|--|
| Nomor Laporan | : SOILTEST - 46.XI. 2020 - MCS |
| Nama Pekerjaan | : SOIL TEST PERENCANAAN GEDUNG DAN BANGUNAN BANK NTB |
| Lokasi | : Kota Mataram - NTB |
| Titik Bor | : BH.2 |
| Koordinat | : - - |
| Jenis Analisa | : Pondasi Dangkal |
| Metode | : Meyerhof |

Data Lapangan (SPT)

| Kedalaman (m) | Nilia SPT (puulan) |
|--------------------|-------------------------|
| 0.00 | 0 |
| 2.00 | 9 |
| 4.00 | 15 |
| 6.00 | 28 |
| 8.00 | 11 |
| 10.00 | 32 |
| 12.00 | 28 |
| 14.00 | 33 |
| 16.00 | 22 |
| 18.00 | 4 |
| 20.00 | 21 |
| 22.00 | 60 |
| 24.00 | 60 |
| 26.00 | 33 |
| 28.00 | 35 |
| 30.00 | 38 |

A. Nilai rata - rata SPT (N50)

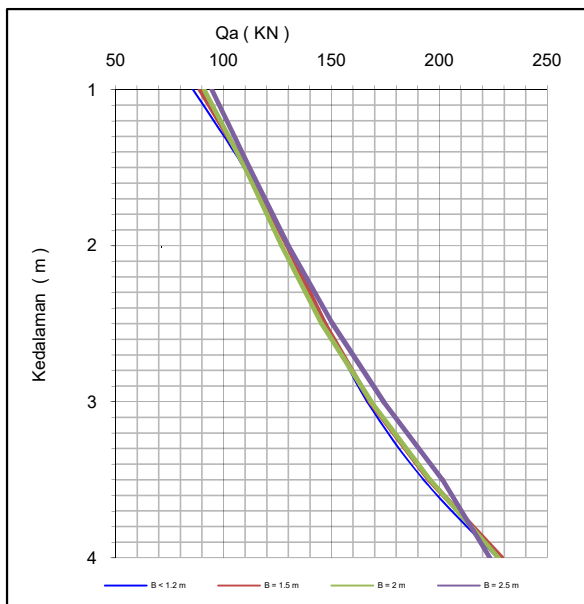
| Kedalaman Pondasi (m) | Jenis Tanah | Lebar Pondasi (B) dalam m' | | | |
|-------------------------------|-----------------|------------------------------|------|------|------|
| | | < 1.2 | 1.50 | 2.00 | 2.50 |
| 1.00 | Lanau Kepasiran | 7 | 8 | 9 | 9 |
| 1.50 | | 9 | 10 | 10 | 11 |
| 2.00 | Pasir Kelanauan | 11 | 11 | 12 | 13 |
| 2.50 | | 12 | 13 | 14 | 15 |
| 3.00 | | 14 | 15 | 16 | 17 |
| 3.50 | | 16 | 17 | 19 | 20 |
| 4.00 | | 19 | 20 | 22 | 22 |

B. Kapasitas Dukung Tanah (q_a)

| Kedalaman Pondasi (m) | Kapasitas Dukung Tanah (q _a) KN/m ² | | | |
|-------------------------------|---|-----------|---------|-----------|
| | B < 1.2 m | B = 1.5 m | B = 2 m | B = 2.5 m |
| 1.00 | 86 | 89 | 91 | 95 |
| 1.50 | 110 | 111 | 110 | 112 |
| 2.00 | 130 | 130 | 127 | 130 |
| 2.50 | 148 | 147 | 145 | 150 |
| 3.00 | 167 | 168 | 168 | 174 |
| 3.50 | 193 | 195 | 196 | 201 |
| 4.00 | 227 | 229 | 227 | 223 |

Penanggung Jawab Lap :

B. Grafik Daya Dukung Ijin Tanah Pondasi Dangkal



Masyhari

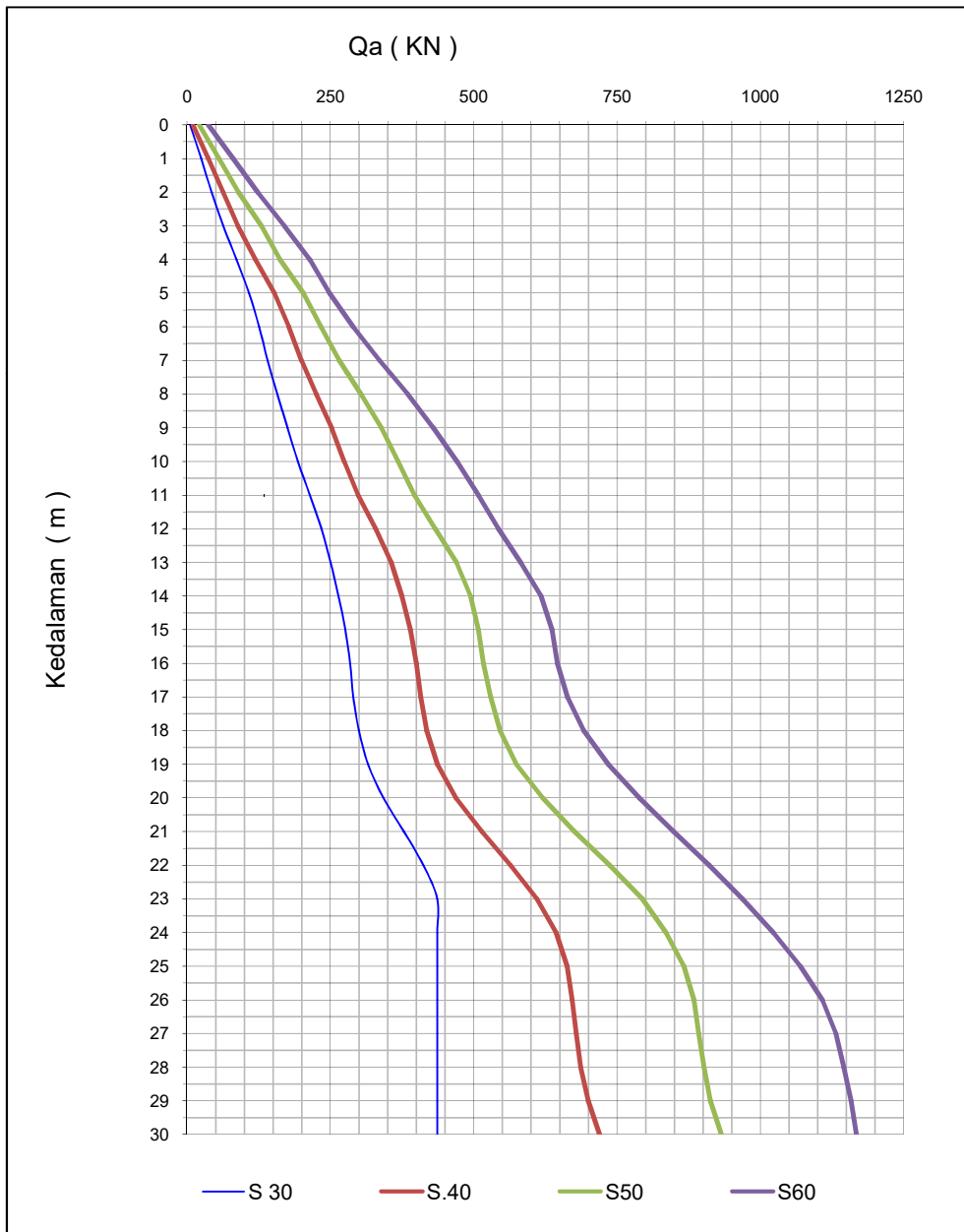
Diperiksa :

Mr.Ikhwan, ST

ANALISA DAYA DUKUNG

| | |
|-----------------------|--|
| Nomor Laporan | : SOILTEST - 46.XI. 2020 - MCS |
| Nama Pekerjaan | : SOIL TEST PERENCANAAN GEDUNG DAN BANGUNAN BANK NTB |
| Lokasi | : Kota Mataram - NTB |
| Titik Bor | : BH.2 |
| Koordinat | : - Elevasi : - |
| Jenis Analisa | : Pondasi Pile |
| Metode | : Meyerhof |
| Data Lapangan (SPT) | Nilai SPT |

B. Grafik Daya Dukung Ijin Tanah Pondasi Dalam (Pile)





PROGRAM STUDI TEKNIK SIPIL
FAKULTAS TEKNIK
UNIVERSITAS MUHAMMADIYAH MATARAM
2023

TUGAS AKHIR / SKRIPSI

DIGAMBAR :

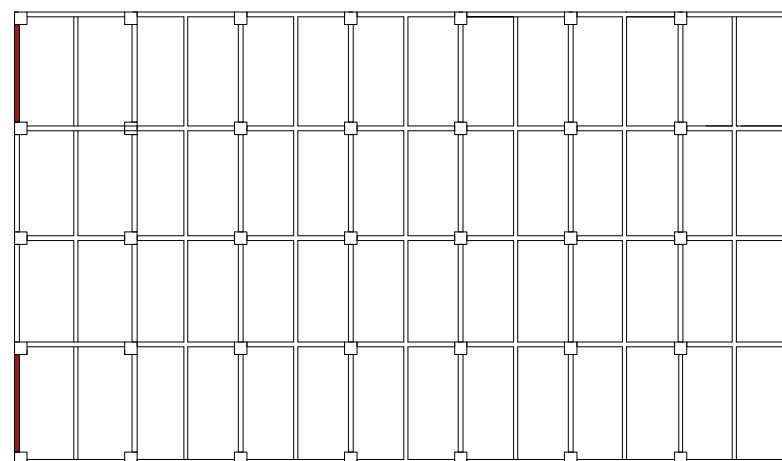
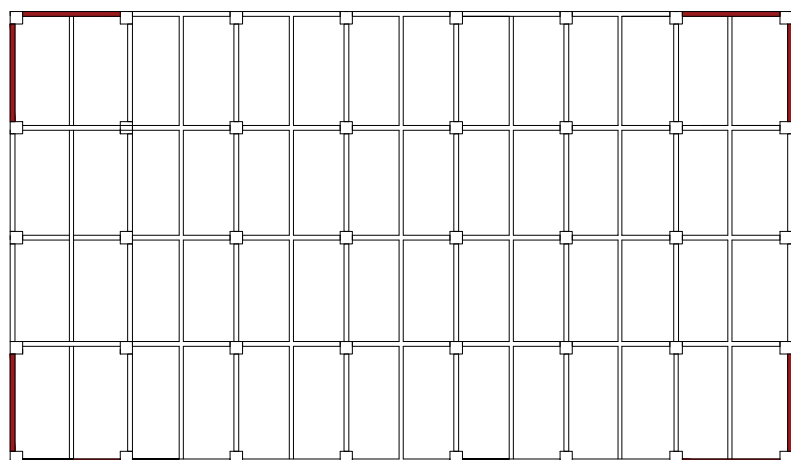
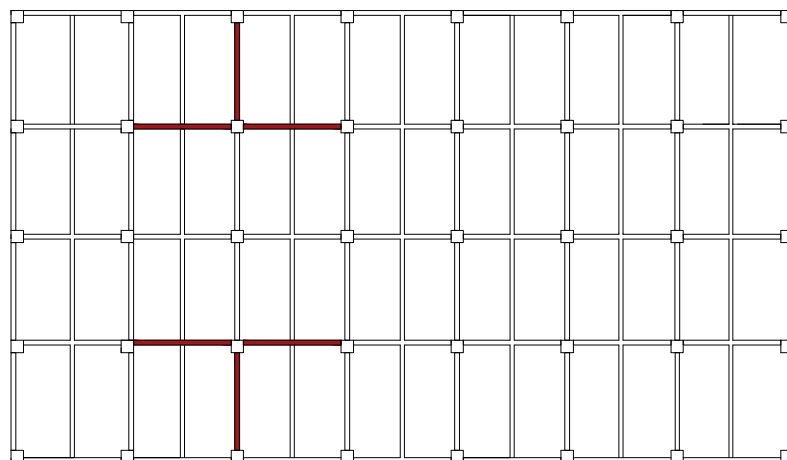
RANNI SAHLINDA
2019D1B161

CATATAN/REVISI :

NAMA GAMBAR :

SKALA :

1:100



| TABLE: Modal Participating Mass Ratios | | | | | | | | | | | | | | | |
|--|----------|----------|----------|-----------|-------------|------------|-----------|----------|-----------|-------------|-------------|-------------|----------|-----------|------------|
| OutputCase | StepType | StepNum | Period | UX | UY | UZ | SumUX | SumUY | SumUZ | RX | RY | RZ | SumRX | SumRY | SumRZ |
| Text | Text | Unitless | Sec | Unitless | Unitless | Unitless | Unitless | Unitless | Unitless | Unitless | Unitless | Unitless | Unitless | Unitless | Unitless |
| MODAL | Mode | 1 | 0,907849 | 1,565E-11 | 0,78413 | 6,235E-09 | 1,565E-11 | 0,78413 | 6,235E-09 | 0,06113 | 1,266E-09 | 0,00001253 | 0,06113 | 1,266E-09 | 0,00001253 |
| MODAL | Mode | 2 | 0,902615 | 0,78494 | 1,613E-11 | 2,051E-12 | 0,78494 | 0,78413 | 6,237E-09 | 4,532E-12 | 0,02649 | 4,224E-14 | 0,06113 | 0,02649 | 0,00001253 |
| MODAL | Mode | 3 | 0,841027 | 6,152E-14 | 0,00001276 | 1,049E-09 | 0,78494 | 0,78415 | 7,286E-09 | 0,000001014 | 2,04E-10 | 0,783 | 0,06113 | 0,02649 | 0,78301 |
| MODAL | Mode | 4 | 0,271416 | 1,753E-09 | 0,10554 | 7,031E-08 | 0,78494 | 0,88968 | 7,76E-08 | 0,12693 | 2,171E-08 | 0,000001277 | 0,18806 | 0,02649 | 0,78301 |
| MODAL | Mode | 5 | 0,2701 | 0,10505 | 1,838E-09 | 2,482E-11 | 0,88999 | 0,88968 | 7,762E-08 | 2,558E-09 | 0,05528 | 1,043E-12 | 0,18806 | 0,08177 | 0,78301 |
| MODAL | Mode | 6 | 0,251751 | 2,656E-12 | 0,000001271 | 2,052E-08 | 0,88999 | 0,88968 | 9,815E-08 | 0,000001921 | 3,863E-09 | 0,10616 | 0,18806 | 0,08177 | 0,88917 |
| MODAL | Mode | 7 | 0,204163 | 1,031E-09 | 0,000005291 | 0,00118 | 0,88999 | 0,88969 | 0,00118 | 0,00072 | 0,00023 | 0,000001272 | 0,18878 | 0,082 | 0,88918 |
| MODAL | Mode | 8 | 0,203705 | 7,41E-10 | 0,000002092 | 0,00123 | 0,88999 | 0,88969 | 0,00241 | 0,00073 | 0,00024 | 6,404E-07 | 0,18951 | 0,08224 | 0,88918 |
| MODAL | Mode | 9 | 0,203559 | 1,688E-11 | 1,67E-08 | 0,00014 | 0,88999 | 0,88969 | 0,00255 | 0,00008677 | 0,0000274 | 3,581E-08 | 0,1896 | 0,08227 | 0,88918 |
| MODAL | Mode | 10 | 0,203424 | 1,585E-10 | 8,205E-07 | 0,00008688 | 0,88999 | 0,88969 | 0,00264 | 0,00004168 | 0,00001694 | 0,0000001 | 0,18964 | 0,08229 | 0,88918 |
| MODAL | Mode | 11 | 0,203313 | 1,295E-09 | 0,000005713 | 0,00002712 | 0,88999 | 0,8897 | 0,00267 | 0,00000529 | 0,000005346 | 7,685E-07 | 0,18965 | 0,08229 | 0,88918 |
| MODAL | Mode | 12 | 0,203241 | 3,757E-09 | 0,000015 | 0,00041 | 0,88999 | 0,88971 | 0,00308 | 0,00013 | 0,00008048 | 0,000003594 | 0,18978 | 0,08237 | 0,88918 |
| MODAL | Mode | 13 | 0,136493 | 2,222E-09 | 0,04789 | 3,076E-08 | 0,88999 | 0,9376 | 0,00308 | 0,02154 | 3,24E-09 | 2,019E-07 | 0,21132 | 0,08237 | 0,88918 |
| MODAL | Mode | 14 | 0,136095 | 0,04775 | 2,19E-09 | 4,379E-12 | 0,93774 | 0,9376 | 0,00308 | 9,329E-10 | 0,00965 | 4,078E-13 | 0,21132 | 0,09202 | 0,88918 |
| MODAL | Mode | 15 | 0,126633 | 4,339E-13 | 1,721E-07 | 4,622E-09 | 0,93774 | 0,9376 | 0,00308 | 9,171E-08 | 9,055E-10 | 0,04815 | 0,21132 | 0,09202 | 0,93733 |

| TABLE: Element Forces - Frames | | | | | | | | | | | | |
|--------------------------------|---------|------------|-------------|----------|----------|--------|---------|------------|---------|---------|-----------|-------------|
| Frame | Station | OutputCase | CaseType | StepType | P | V2 | V3 | T | M2 | M3 | FrameElem | ElemStation |
| Text | m | Text | Text | Text | KN | KN | KN | KN-m | KN-m | KN-m | Text | m |
| 887 | 3,5 | EVENLOP | Combination | Max | 1375,149 | -0,431 | -5,674 | 0,00001064 | 27,6138 | 2,4411 | 887-1 | 3,5 |
| 892 | 3,5 | EVENLOP | Combination | Max | 878,535 | -2,224 | -11,454 | 0,00002936 | 42,784 | 9,517 | 892-1 | 3,5 |
| 897 | 4 | EVENLOP | Combination | Max | 1124,868 | -1,044 | -8,484 | 0,00002166 | 33,2798 | 5,347 | 897-1 | 4 |
| 917 | 3,5 | EVENLOP | Combination | Max | 171,795 | -4,787 | -18,425 | 0,00002601 | 79,6091 | 22,1386 | 917-1 | 3,5 |
| 927 | 3,5 | EVENLOP | Combination | Max | 407,506 | -2,766 | -10,56 | 0,00002195 | 35,0032 | 10,4419 | 927-1 | 3,5 |
| 928 | 3,5 | EVENLOP | Combination | Max | 643,001 | -2,381 | -10,5 | 0,00001986 | 40,4382 | 10,3611 | 928-1 | 3,5 |

BALOK TEPI

| | | | | | | | | | | | | |
|-----|---|---------|-------------|-----|---|--------|----------|--------|----------|----------|-------|---|
| 35 | 8 | EVENLOP | Combination | Max | 0 | 62,373 | 8,58E-20 | 3,316 | 3,81E-19 | -45,7521 | 35-2 | 4 |
| 141 | 8 | EVENLOP | Combination | Max | 0 | 65,188 | 2,48E-19 | 3,5208 | 8,11E-19 | -47,6812 | 141-2 | 4 |
| 331 | 8 | EVENLOP | Combination | Max | 0 | 64,563 | 4,60E-19 | 3,6537 | 1,56E-18 | -47,2851 | 331-2 | 4 |
| 426 | 8 | EVENLOP | Combination | Max | 0 | 64,683 | 4,26E-20 | 3,735 | 1,44E-18 | -47,4065 | 426-2 | 4 |
| 521 | 8 | EVENLOP | Combination | Max | 0 | 64,724 | 8,90E-19 | 3,8999 | 1,76E-18 | -47,434 | 521-2 | 4 |
| 616 | 8 | EVENLOP | Combination | Max | 0 | 44,258 | 1,55E-18 | 3,8634 | 6,35E-18 | -33,7481 | 616-2 | 4 |

BALOK TENGAH

| | | | | | | | | | | | | |
|-----|---|---------|-------------|-----|---|--------|-----------|------------|-----------|----------|-------|---|
| 63 | 8 | EVENLOP | Combination | Max | 0 | 56,655 | 1,23E-19 | 0,0004164 | 4,94E-19 | -46,3288 | 63-2 | 4 |
| 63 | 8 | EVENLOP | Combination | Min | 0 | 28,731 | -1,24E-19 | -0,0003841 | -4,92E-19 | -91,3579 | 63-2 | 4 |
| 163 | 8 | EVENLOP | Combination | Max | 0 | 56,779 | 0 | 0,0006771 | 4,40E-19 | -46,4541 | 163-2 | 4 |
| 163 | 8 | EVENLOP | Combination | Min | 0 | 28,794 | 0 | -0,0004356 | -4,38E-19 | -91,6067 | 163-2 | 4 |
| 353 | 8 | EVENLOP | Combination | Max | 0 | 56,879 | 7,62E-19 | 0,0008174 | 1,98E-18 | -46,5549 | 353-2 | 4 |
| 353 | 8 | EVENLOP | Combination | Min | 0 | 28,845 | -7,65E-19 | -0,0004783 | -1,97E-18 | -91,8064 | 353-2 | 4 |
| 448 | 8 | EVENLOP | Combination | Max | 0 | 56,968 | 7,76E-19 | 0,000879 | 2,93E-18 | -46,6451 | 448-2 | 4 |
| 448 | 8 | EVENLOP | Combination | Min | 0 | 28,89 | -7,74E-19 | -0,0004666 | -2,93E-18 | -91,9844 | 448-2 | 4 |
| 543 | 8 | EVENLOP | Combination | Max | 0 | 57,036 | 8,82E-19 | 0,0009355 | 1,76E-18 | -46,7153 | 543-2 | 4 |
| 543 | 8 | EVENLOP | Combination | Min | 0 | 28,924 | -8,77E-19 | -0,0004042 | -1,78E-18 | -92,1226 | 543-2 | 4 |
| 638 | 8 | EVENLOP | Combination | Max | 0 | 57,194 | 1,55E-18 | 0,0006712 | 6,33E-18 | -46,8727 | 638-2 | 4 |
| 638 | 8 | EVENLOP | Combination | Min | 0 | 29,005 | -1,54E-18 | -0,000289 | -6,33E-18 | -92,431 | 638-2 | 4 |

KOLOM TENGAH

| TABLE: Element Forces - Frames | | | | | | | | | | | | |
|--------------------------------|---------|------------|-------------|----------|-----------|--------|----------|---------|-------|---------|-----------|-------------|
| Frame | Station | OutputCase | CaseType | StepType | P | V2 | V3 | T | M2 | M3 | FrameElem | ElemStation |
| Text | mm | Text | Text | Text | KN | KN | KN | KN-mm | KN-mm | KN-mm | Text | mm |
| 784 | 3500 | EVENLOP | Combination | Max | -1394,533 | 0,011 | 0,01 | 0,02936 | 7,46 | 27,19 | 784-1 | 3500 |
| 792 | 4000 | EVENLOP | Combination | Max | -1764,348 | 0,057 | 0,005274 | 0,02166 | 3,74 | -24,19 | 792-1 | 4000 |
| 793 | 3500 | EVENLOP | Combination | Max | -2140,908 | 0,072 | 0,008745 | 0,01064 | 4,2 | -81,69 | 793-1 | 3500 |
| 818 | 3500 | EVENLOP | Combination | Max | -314,518 | 0,548 | 0,013 | 0,02601 | 7,06 | -618,71 | 818-1 | 3500 |
| 824 | 3500 | EVENLOP | Combination | Max | -1034,687 | 0,118 | 0,009433 | 0,01986 | 7,43 | -89,18 | 824-1 | 3500 |
| 826 | 3500 | EVENLOP | Combination | Max | -674,597 | -0,026 | 0,011 | 0,02195 | 10,37 | 283,63 | 826-1 | 3500 |

Table: Joint Displacements Tanpa Dinding Geser

| TABLE: Joint Displacements | | | | | | | | | |
|----------------------------|------------|------------|----------|----------|----------|----------|----------|----------|----------|
| Joint | OutputCase | CaseType | StepType | U1 | U2 | U3 | R1 | R2 | R3 |
| Text | Text | Text | Text | mm | mm | mm | Radians | Radians | Radians |
| 40 | DX | LinRespSpe | Max | 2,244997 | 0,000047 | 0,047893 | 4,74E-07 | 0,00102 | 7,02E-11 |
| 40 | DY | LinRespSpe | Max | 0,0094 | 2,247312 | 0,050597 | 0,001018 | 3,11E-06 | 5,87E-07 |
| 122 | DX | LinRespSpe | Max | 7,457071 | 0,000121 | 0,092731 | 5,48E-07 | 0,001314 | 1,98E-10 |
| 122 | DY | LinRespSpe | Max | 0,031658 | 7,475312 | 0,098014 | 0,001316 | 4,22E-06 | 1,98E-06 |
| 272 | DX | LinRespSpe | Max | 12,19319 | 0,000142 | 0,120747 | 6,19E-07 | 0,001247 | 2,64E-10 |
| 272 | DY | LinRespSpe | Max | 0,0523 | 12,23745 | 0,127676 | 0,001251 | 3,89E-06 | 3,27E-06 |
| 347 | DX | LinRespSpe | Max | 16,48032 | 0,000126 | 0,142793 | 7,33E-07 | 0,001008 | 2,91E-10 |
| 347 | DY | LinRespSpe | Max | 0,071098 | 16,55655 | 0,151054 | 0,001012 | 2,91E-06 | 4,44E-06 |
| 422 | DX | LinRespSpe | Max | 19,61618 | 0,000138 | 0,154155 | 3,84E-07 | 0,000673 | 3,4E-10 |
| 422 | DY | LinRespSpe | Max | 0,084978 | 19,7273 | 0,163137 | 0,00068 | 2,09E-06 | 5,31E-06 |
| 497 | DX | LinRespSpe | Max | 21,55409 | 0,000198 | 0,158399 | 7,86E-07 | 0,000431 | 4,18E-10 |
| 497 | DY | LinRespSpe | Max | 0,093725 | 21,70096 | 0,167649 | 0,000436 | 1,59E-06 | 5,85E-06 |
| 540 | DX | LinRespSpe | Max | 0 | 0 | 0 | 0 | 0 | 0 |
| 540 | DY | LinRespSpe | Max | 0 | 0 | 0 | 0 | 0 | 0 |

Table: Joint Displacements Dinding Geser Alternatif 1

| TABLE: Joint Displacements | | | | | | | | | |
|----------------------------|------------|------------|----------|----------|----------|----------|----------|----------|----------|
| Joint | OutputCase | CaseType | StepType | U1 | U2 | U3 | R1 | R2 | R3 |
| Text | Text | Text | Text | mm | mm | mm | Radians | Radians | Radians |
| 32 | DX | LinRespSpe | Max | 0,00004 | 1,07E-10 | 0,00003 | 1,98E-09 | 1,39E-08 | 4,13E-16 |
| 32 | DY | LinRespSpe | Max | 1,45E-10 | 0,000075 | 3,47E-06 | 3,06E-08 | 1,01E-09 | 6,1E-15 |
| 114 | DX | LinRespSpe | Max | 0,000123 | 3,74E-10 | 0,000055 | 1,78E-09 | 2,04E-08 | 2,11E-15 |
| 114 | DY | LinRespSpe | Max | 3,93E-10 | 0,000219 | 7,79E-06 | 4,43E-08 | 2,64E-09 | 1,74E-14 |
| 264 | DX | LinRespSpe | Max | 0,000211 | 6,14E-10 | 0,000068 | 7,42E-09 | 2,31E-08 | 3,51E-15 |
| 264 | DY | LinRespSpe | Max | 6,66E-10 | 0,000377 | 0,000011 | 4,75E-08 | 2,82E-09 | 3E-14 |
| 339 | DX | LinRespSpe | Max | 0,000309 | 9,36E-10 | 0,000076 | 8,63E-09 | 2,7E-08 | 6,06E-15 |
| 339 | DY | LinRespSpe | Max | 9,58E-10 | 0,000553 | 0,000013 | 6,17E-08 | 4,96E-09 | 4,56E-14 |
| 414 | DX | LinRespSpe | Max | 0,000407 | 1,27E-09 | 0,000078 | 1,78E-08 | 2,52E-08 | 9,01E-15 |
| 414 | DY | LinRespSpe | Max | 1,24E-09 | 0,00073 | 0,000015 | 5,15E-08 | 5,36E-09 | 6,11E-14 |
| 489 | DX | LinRespSpe | Max | 0,000495 | 1,5E-09 | 0,000077 | 4,55E-08 | 2,45E-08 | 1,09E-14 |
| 489 | DY | LinRespSpe | Max | 1,51E-09 | 0,000883 | 0,000014 | 9,13E-08 | 6,74E-09 | 7,55E-14 |
| 539 | DX | LinRespSpe | Max | 0 | 0 | 0 | 0 | 0 | 0 |
| 539 | DY | LinRespSpe | Max | 0 | 0 | 0 | 0 | 0 | 0 |

Table: Joint Displacements Dinding Geser Alternatif 2

| TABLE: Joint Displacements | | | | | | | | | |
|----------------------------|------------|------------|----------|----------|----------|----------|----------|----------|----------|
| Joint | OutputCase | CaseType | StepType | U1 | U2 | U3 | R1 | R2 | R3 |
| Text | Text | Text | Text | mm | mm | mm | Radians | Radians | Radians |
| 40 | DX | LinRespSpe | Max | 2,251509 | 5,51E-06 | 0,021952 | 1,61E-07 | 0,001032 | 2,29E-10 |
| 40 | DY | LinRespSpe | Max | 2,93E-06 | 0,339611 | 0,288621 | 0,000121 | 1,55E-06 | 5,48E-11 |
| 122 | DX | LinRespSpe | Max | 7,492854 | 0,000011 | 0,042643 | 1,71E-07 | 0,001331 | 4,48E-10 |
| 122 | DY | LinRespSpe | Max | 2,85E-06 | 1,022414 | 0,529927 | 0,000166 | 2,85E-06 | 1,66E-10 |
| 272 | DX | LinRespSpe | Max | 12,26527 | 0,000011 | 0,055703 | 2,51E-07 | 0,001265 | 4,66E-10 |
| 272 | DY | LinRespSpe | Max | 5,35E-06 | 1,739672 | 0,663893 | 0,000195 | 3,99E-06 | 2,83E-10 |
| 347 | DX | LinRespSpe | Max | 16,58197 | 7,62E-06 | 0,064771 | 1,39E-07 | 0,001028 | 2,9E-10 |
| 347 | DY | LinRespSpe | Max | 6,5E-06 | 2,519813 | 0,75165 | 0,000211 | 6,37E-06 | 4,07E-10 |
| 422 | DX | LinRespSpe | Max | 19,74413 | 1,7E-06 | 0,069518 | 2,46E-07 | 0,000686 | 7,18E-11 |
| 422 | DY | LinRespSpe | Max | 9,04E-06 | 3,297157 | 0,786381 | 0,000204 | 4,27E-06 | 5,33E-10 |
| 497 | DX | LinRespSpe | Max | 21,7064 | 9,55E-06 | 0,071284 | 5,52E-08 | 0,000445 | 4,1E-10 |
| 497 | DY | LinRespSpe | Max | 0,000011 | 4,015237 | 0,792991 | 0,000202 | 0,000014 | 6,55E-10 |
| 540 | DX | LinRespSpe | Max | 0 | 0 | 0 | 0 | 0 | 0 |
| 540 | DY | LinRespSpe | Max | 0 | 0 | 0 | 0 | 0 | 0 |

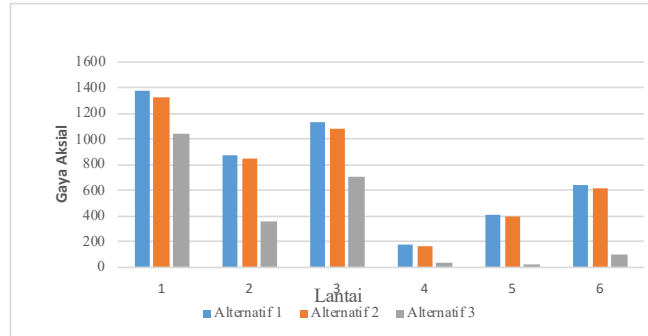
Table: Joint Displacements Dinding Geser Alternatif 3

| TABLE: Joint Displacements | | | | | | | | | |
|----------------------------|------------|------------|----------|----------|----------|----------|----------|----------|----------|
| Joint | OutputCase | CaseType | StepType | U1 | U2 | U3 | R1 | R2 | R3 |
| Text | Text | Text | Text | mm | mm | mm | Radians | Radians | Radians |
| 40 | DX | LinRespSpe | Max | 0,283194 | 1,55E-06 | 0,005633 | 5,32E-08 | 0,000109 | 3,03E-11 |
| 40 | DY | LinRespSpe | Max | 0,479443 | 1,269306 | 0,019033 | 0,000546 | 0,000206 | 0,00003 |
| 122 | DX | LinRespSpe | Max | 0,761854 | 1E-06 | 0,010991 | 4,92E-08 | 0,000119 | 5,05E-11 |
| 122 | DY | LinRespSpe | Max | 1,477073 | 3,940642 | 0,037102 | 0,000667 | 0,00025 | 0,000092 |
| 272 | DX | LinRespSpe | Max | 1,212169 | 1,74E-06 | 0,014644 | 6,36E-08 | 0,000123 | 8,4E-11 |
| 272 | DY | LinRespSpe | Max | 2,38943 | 6,388019 | 0,048957 | 0,000653 | 0,000245 | 0,000149 |
| 347 | DX | LinRespSpe | Max | 1,666597 | 1,93E-06 | 0,017913 | 8,74E-08 | 0,000117 | 2,74E-11 |
| 347 | DY | LinRespSpe | Max | 3,26691 | 8,743401 | 0,05907 | 0,00058 | 0,000218 | 0,000204 |
| 422 | DX | LinRespSpe | Max | 2,085227 | 1,46E-06 | 0,019911 | 5,89E-08 | 0,000104 | 3,38E-11 |
| 422 | DY | LinRespSpe | Max | 4,004848 | 10,72235 | 0,064882 | 0,000457 | 0,000172 | 0,00025 |
| 497 | DX | LinRespSpe | Max | 2,438596 | 2,24E-06 | 0,020767 | 1,45E-07 | 0,000082 | 8,94E-11 |
| 497 | DY | LinRespSpe | Max | 4,556195 | 12,1978 | 0,06725 | 0,000331 | 0,000126 | 0,000285 |
| 540 | DX | LinRespSpe | Max | 0 | 0 | 0 | 0 | 0 | 0 |
| 540 | DY | LinRespSpe | Max | 0 | 0 | 0 | 0 | 0 | 0 |

p

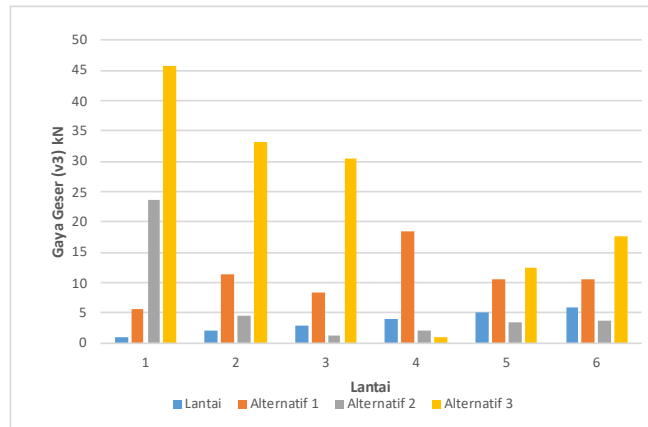
GAYA AKSIAL

| Lantai | Alternatif 1 | Alternatif 2 | Alternatif 3 |
|-----------|--------------|--------------|--------------|
| 1 | 1375,149 | 1325,957 | 1040,672 |
| 2 | 878,535 | 845,235 | 352,662 |
| 3 | 1124,868 | 1082,744 | 704,632 |
| 4 | 171,795 | 165,798 | 39,633 |
| 5 | 407,506 | 392,874 | 25,982 |
| 6 | 643,001 | 619,196 | 104,135 |
| Rata-rata | 766,809 | 4431,804 | 2267,716 |



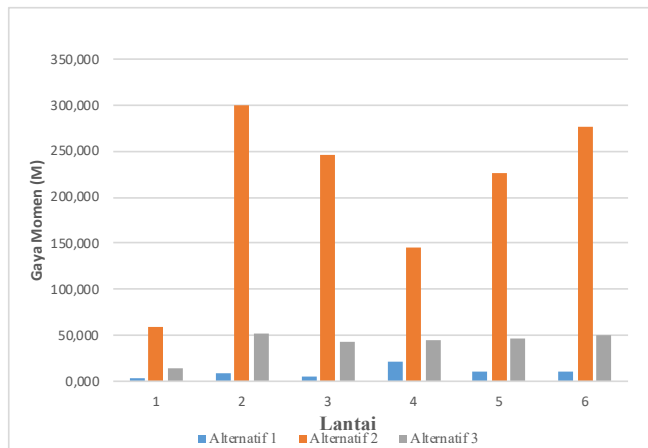
GAYA GESER KOLOM TEPI

| Lantai | Alternatif 1 | Alternatif 2 | Alternatif 3 |
|-----------|--------------|--------------|--------------|
| 1 | 5,674 | 23,501 | 45,814 |
| 2 | 11,454 | 4,619 | 33,094 |
| 3 | 8,484 | 1,192 | 30,487 |
| 4 | 18,425 | 2,135 | 1,131 |
| 5 | 10,56 | 3,455 | 12,406 |
| 6 | 10,5 | 3,738 | 17,725 |
| Rata-rata | 10,8495 | 6,44 | 23,443 |



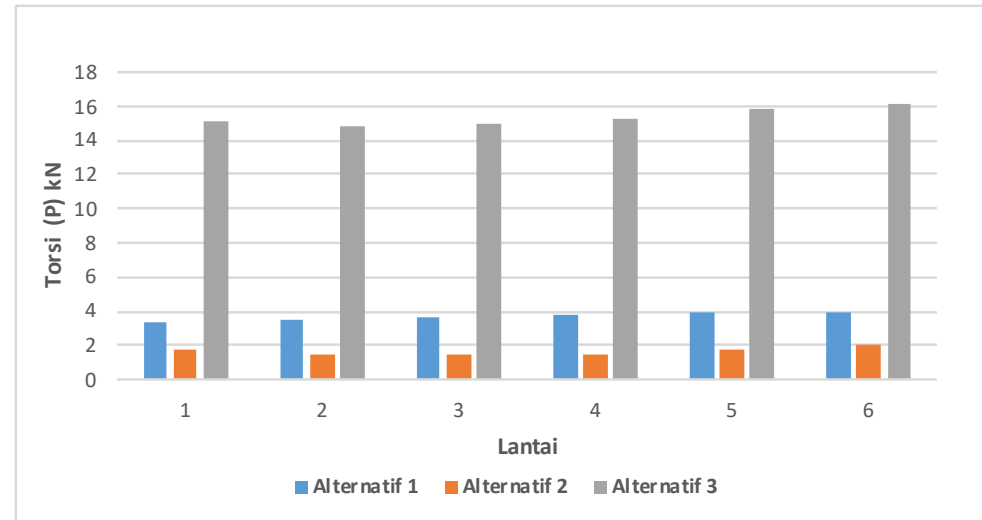
GAYA MOMEN KOLOM TEPI

| Lantai | Alternatif 1 | Alternatif 2 | Alternatif 3 |
|-----------|--------------|--------------|--------------|
| 1 | 2,441 | 59,585 | 14,987 |
| 2 | 9,517 | 300,055 | 52,090 |
| 3 | 5,347 | 245,251 | 41,975 |
| 4 | 22,139 | 144,817 | 44,346 |
| 5 | 10,442 | 225,407 | 47,002 |
| 6 | 10,361 | 276,009 | 49,775 |
| Rata-rata | 10,041 | 208,521 | 41,696 |



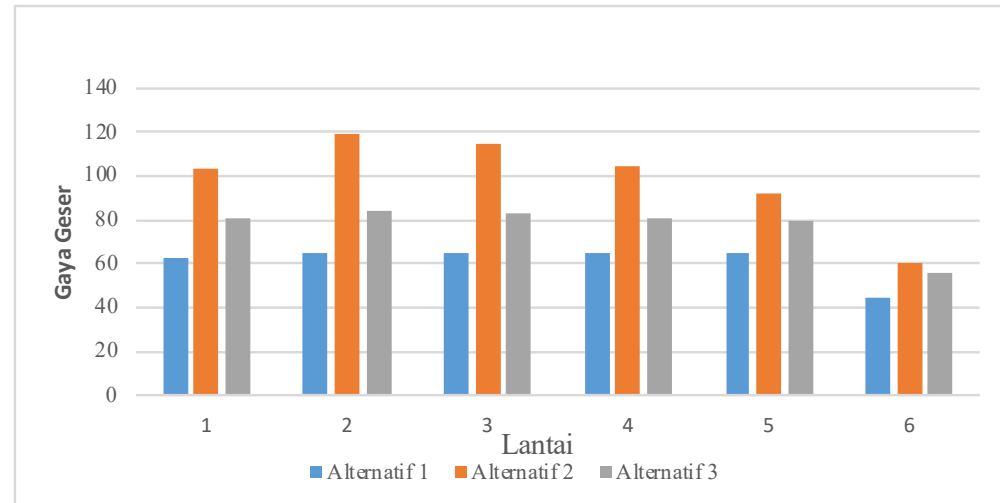
Gaya Torsi

| Lantai | Alternatif 1 | Alternatif 2 | Alternatif 3 |
|-----------|--------------|--------------|--------------|
| 1 | 3,316 | 1,751 | 15,1246 |
| 2 | 3,5208 | 1,5048 | 14,9002 |
| 3 | 3,6537 | 1,4149 | 15,0306 |
| 4 | 3,735 | 1,4581 | 15,3172 |
| 5 | 3,8999 | 1,6859 | 15,8427 |
| 6 | 3,8634 | 2,073 | 16,1867 |
| Rata-rata | 3,6648 | 9,8877 | 15,4003 |



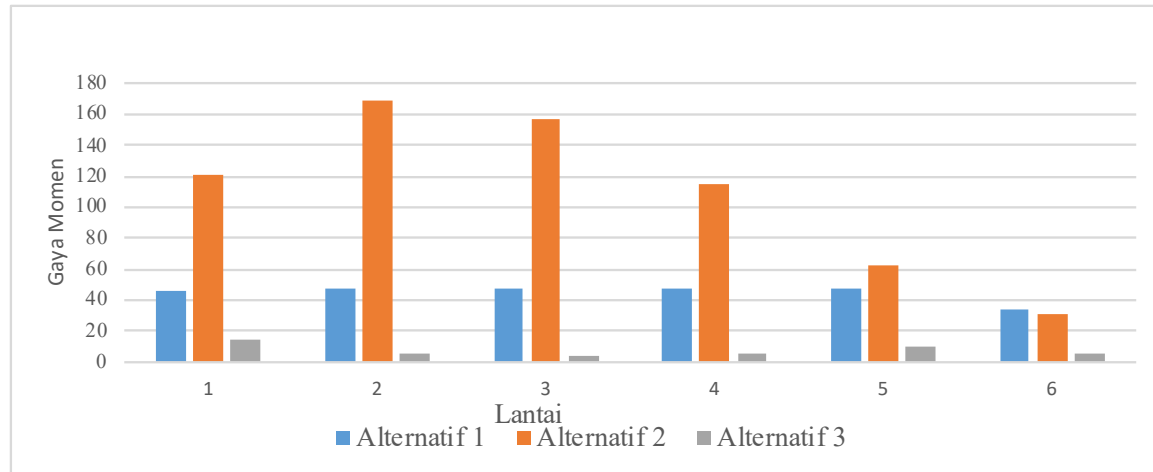
Gaya Geser

| Lantai | Alternatif 1 | Alternatif 2 | Alternatif 3 |
|-----------|--------------|--------------|--------------|
| 1 | 62,373 | 103,671 | 81,013 |
| 2 | 65,188 | 119,073 | 84,662 |
| 3 | 64,563 | 115,269 | 83,139 |
| 4 | 64,683 | 104,693 | 81,258 |
| 5 | 64,724 | 91,954 | 79,325 |
| 6 | 44,258 | 59,943 | 56,258 |
| Rata-rata | 60,965 | 99,101 | 77,609 |



Gaya Momen

| Lantai | Alternatif 1 | Alternatif 2 | Alternatif 3 |
|-----------|--------------|--------------|--------------|
| 1 | 45,7521 | 120,9556 | 14,691 |
| 2 | 47,6812 | 169,3495 | 5,6832 |
| 3 | 47,2851 | 157,1063 | 3,4663 |
| 4 | 47,4065 | 114,3208 | 5,9782 |
| 5 | 47,434 | 62,9567 | 10,3822 |
| 6 | 33,7481 | 31,1945 | 5,1649 |
| Rata-rata | 44,885 | 109,314 | 7,5610 |



perbandingan displacment akibat beban gempa arah x

| lantai | Shear wall 1 | Shear wall 2 | Shear wall 3 |
|--------|--------------|--------------|--------------|
| base | 0 | 0 | 0 |
| 1 | 0,00004 | 2,2515 | 0,283194 |
| 2 | 0,000123 | 7,49285 | 0,761854 |
| 3 | 0,000211 | 12,265266 | 1,212169 |
| 4 | 0,000309 | 16,5819 | 1,666597 |
| 5 | 0,000407 | 19,74412 | 2,085227 |
| 6 | 0,000495 | 21,7063 | 2,438596 |

perbandingan displacment akibat beban gempa arah y

| lantai | Shear wall 1 | Shear wall 2 | Shear wall 3 |
|--------|--------------|--------------|--------------|
| base | 0 | 0 | 0 |
| 1 | 0,000075 | 0,339611 | 1,269306 |
| 2 | 0,000219 | 1,02241 | 3,940642 |
| 3 | 0,000377 | 1,73967 | 6,388019 |
| 4 | 0,000553 | 2,51981 | 8,743401 |
| 5 | 0,00073 | 3,29715 | 10,722351 |
| 6 | 0,000883 | 4,01523 | 12,197796 |

